

FESHM 5031.1 PIPING ENGINEERING NOTE FORM

Prepared by: Mark Adamowski & Terry Tope Preparation Date: July 18th, 2011

Piping System Title: LAPD LN2 and LAr Supply Piping

Lab Location: PC4

Lab Location code: 701030125

Purpose of system / System description: To supply liquid nitrogen and liquid argon to LAPD.

Piping System ID Number:

Appropriate governing piping code: ASME B31.3 - 2010

Fluid Service Category (if B31.3): Category-D Normal Category-M / High Pressure
(circle one)

Fluid Contents: Liquid & Gaseous Nitrogen and Argon

Design Pressure: 100 psig and 60 psig.

Design Temperature: -320 °F (77 K),

Piping Materials: See Note.

Drawing Numbers (PID's, weldments, etc.): See note.

Designer/Manufacturer: FERMILAB

Test Pressure: See note.

Test Fluid: pneumatic Test Date: See note.

Statements of Compliance

Piping system conforms to FESHM 5031.1, installation *is not* exceptional Yes /
No

Piping system conforms to FESHM 5031.1, installation *is* exceptional and has been designed, fabricated, inspected, and tested using sound engineering principles: Yes / No

Reviewer's Signature: Roger Rabehl ROGER RABEHL Date: 9/7/11

D/S Head's Signature: Wm. W. May

Date: 9/12/2011

ES&H Director's Signature: NA

Date:

(if exceptional)

Director's Signature or Designee: NA

Date:

(if exceptional)

Pipe Characteristics

Size: See note for full details. Primary sections are 1" Type K Copper with foam insulation.

Length: See note for full details. LN2 supply 150 feet. LAr supply 70 feet.

Volume: 40 liters

Relief Valve Information

Type: See Note

Manufacturer:

Set Pressure:

Relief Capacity:

Relief Design Code:

Is the system designed to meet the identified governing code? Yes / No

Fabrication Quality Verification

System Documentation

Process and Instrumentation diagram appended?

Yes No

Process and Instrumentation component list appended?

Yes No

Is an operating procedure necessary for safe operation?
If 'yes', procedure must be appended.

Yes No

Exceptional Piping System

Is the piping system or any part of it in the above category?

Yes No

If "Yes", follow the requirements for an extended engineering note for Exceptional Piping Systems.

Quality Assurance

List vendor(s) for assemblies welded/brazed off site: No assemblies were fabricated off site.

List welder(s) for assemblies welded/brazed in-house: See Note.

Append welder qualification records for in-house welded/brazed assemblies. See note appendix.

Append all quality verification records required by the identified code (e.g. examiner's certification, inspector's certification, test records, etc.)

<http://lartpc-docdb.fnal.gov:8080/cgi-bin>ShowDocument?docid=639>

Statements of Compliance for Amendment #1

Prepared by: Terry Tope

Preparation Date: June 25, 2012

Piping system conforms to FESHM 5031.1, installation **is not** exceptional Yes /
No

Piping system conforms to FESHM 5031.1, installation **is** exceptional and has been designed, fabricated, inspected, and tested using sound engineering principles: Yes / No

Reviewer's Signature: Roger Rabehl Date: 11/9/12

D/S Head's Signature: Matt Zingg Date: 11/12/2012

ES&H Director's Signature: NA _____ Date: _____
(if exceptional)

Director's Signature or Designee: NA _____ Date: _____
(if exceptional)



Particle Physics Division

Mechanical Department Engineering Note

Number: LArTPC DOC-553

Date: 06/25/12

Project Internal Reference:

Project: LAPD

Title: LAPD LN2 Supply and LAr Supply Piping Engineering Note

Author(s): Mark Adamowski, Terry Tope

Reviewer(s): Key Words: LAPD, LN2, LAr, Piping

Abstract Summary:

This note documents the liquid nitrogen, gaseous nitrogen, and liquid argon supply piping for LAPD. The note has been amended to document the changes implemented in preparation for LAPD Run 2.

Applicable Codes:

1. *Fermilab Piping Systems, FESHM Chapter 5031.1, Rev. 11/ 2007*
2. *ASME B31.3-2010*

1. INTRODUCTION

Nitrogen liquid and gas are used for LAPD, located in PC4. Liquid nitrogen is used as a coolant for the Argon condenser. A nitrogen phase separator is used to vent off any boil-off nitrogen before the argon condenser. The nitrogen gas from the condenser is vented outside.

Nitrogen gas is generated outside with an ambient vaporizer. The vaporized nitrogen gas is supplied to the filter regeneration system. This demand for nitrogen gas is expected to be sporadic as needed based on filter life.

The nitrogen will also provide foam insulation purges. Total maximum purge rate is 5 SCFH.

The design pressure for the majority of the N2 piping is 100 psig which is the highest differential pressure for the solenoid valves. A small portion of the piping has a design pressure of 60 psig due to the 60 psig MAWP of the condenser vessel which makes pressure testing the attached piping at 100 psig impossible. All calculations are performed for 100 psig, thus they are adequate for the 60 psig portions. The LN2 supply trailer has a MAWP of 50 psig thus the nitrogen source cannot over pressurize the system.

The liquid argon supply piping for filling the LAPD tank is constructed in the same manner as the liquid nitrogen supply piping and is also included in this note. The liquid argon supply contract stipulates that the vendor tanker will have an MAWP less than or equal to 75 psig and the tanker liquid pump can be locked out. Thus a 100 psig design pressure for the liquid argon supply piping ensures it cannot be over pressurized by the source.

A tie in to supply liquid nitrogen to the LBNE 35T cryostat has been added to the LAPD liquid nitrogen supply inside PC4. The flow schematic in Appendix 1 notes these additions. The addition includes two liquid nitrogen isolation valves, four room temperature instrument isolation valves, two pressure gauges, a pressure transmitter, a strainer, and two trapped volume reliefs.

2. FLOW SCHEMATIC

The N2 and LAr supply piping and instrumentation is part of the LAPD P&ID¹. The N2 piping appears on P&ID sheet 1, rows G, H columns 2 through 8, and sheet 2, rows F through H and columns 4 through 8. The LAr supply piping appears on P&ID sheet 3, rows G and F and

¹ Liquid Argon Purity Demonstration (LAPD) Cryogenic Safety Report, Section 1.2, LArTPC-Docdb-553.

columns 1 thru 3. In Appendix 1 the relevant piping sections are highlighted on the flow schematic along with their design and test pressures. The new components associated with the amendment are boxed on sheet 1 of the annotated flow schematic.

3. DESIGN CODE

The N2 and LAr supply piping to LAPD must meet the requirements of FESHM 5031.1. Cryogenic liquid is covered by ASME B31.3, Normal Fluid Service. Nitrogen vapor piping downstream of SV-144-N2 is considered Category D Fluid Service and outside of the scope of this note because its design temperature is above -20 F (and its design pressure is less than 150 psig). TE-146-N located at the outlet of the ambient liquid nitrogen vaporizer is monitored by the PLC. The PLC will close SV-144-N2 if TE-146-N drops below -20 F. The ambient vaporizer is rated to deliver 5,200 SCFH at 70 F for 8 hours with a 20 F approach to ambient. Nitrogen system demand is not expected to exceed 500 SCFH nor is demand at the 500 SCFH level expected to exceed 8 hours such that it is unlikely that the vaporizer will deliver gas colder than -20 F at its outlet. The piping from SV-144-N2 is considered in the flexibility analysis up to the 1st hard fixed point inside PC4.

4. MATERIALS

The majority of the LN2 and LAr supply piping is fabricated from pre-insulated type K copper tubing. Some of the connecting components are bronze and some are 304/316 stainless steel. Of the materials involved, the copper tubing has the lowest allowable stress of 6000 psi².

The N2 gas supply piping is fabricated from un-insulated copper tubing.

The lowest temperature for LN2 is 77 K and 87 K is the lowest for LAr. This temperature is above the minimum temperature for copper (4.3 K) and 304/316 (19.3 K).

The Nitrogen and Argon valves and instruments are included in the LAPD valve and instrument list, which is available in Appendix 1.

Components not conforming to the standards in B31.3 Table 326.1 are listed in Table 1.

The amendment does not introduce additional unlisted components.

² Per B31.3, Table A-1.

Table 1: Unlisted Components

Component	Manufacturer	Classification	Pressure rating	System design pressure	Comments
			psig	psig	
Braided metal flexible hose - 1 in. dia.	Hosemaster	Unlisted	718	100	See note 1
VCR fittings	Swagelok	Unlisted	1900	100	See note 2
Tube weld fittings	Swagelok	Unlisted	2400	100	See note 3
Compression fittings	Swagelok	Unlisted	1450	100	See note 4
Vaporizer	Thermax	Unlisted	600	100	See note 5
Tube socket weld elbows - 3/4 in. dia.	Truly Tubular	Unlisted	8285	100	See note 6
Fermilab 1/2" cryo control valve	FNAL	Unlisted	350	100	See note 7

Notes

- 1 Hosemaster supplies a pressure rating for these Masterflex hoses and extensive service experience exists for both liquid nitrogen and liquid argon.
- 2 The lowest pressure rating of any Swagelok VCR fitting is 1900 psi. Extensive service experience exists for Swagelok VCR fittings in liquid argon service at pressures up to 415 psid.
- 3 The lowest pressure rating of any Swagelok tube weld fitting is 2400 psi. Extensive service experience exists for Swagelok tube weld fittings in liquid argon service at pressures up to 415 psid.
- 4 The lowest pressure rating of any Swagelok compression fitting is 1813 psi.
- 5 The manufacturer supplied pressure rating is 600 psi for a Thermax SG50HF with male pipe thread fittings.
- 6 Truly Tubular pressure ratings are defined as the minimum pressure which would cause permanent deformation.
- 7 Fermilab 1/2" cryogenic control valves have been operated on 350 psi systems extensively.

5. DESIGN PRESSURE AND MINIMUM TUBE WALL

Solenoids are used in the nitrogen supply piping. The largest pressure differential for under which these solenoid can still open / close is 100 psig. This will be used as the design pressure for the both the nitrogen and argon piping.

The liquid nitrogen supply and liquid argon supply piping are fabricated from pre-insulated 1 inch, type K, copper tubing. The vapor supply nitrogen piping is fabricated from bare 1 inch, type K copper tubing.

The required tubing wall thickness is 0.009 inch for the 100 psig design pressure. The minimum wall thickness calculations are detailed in the Appendix 2. Type K, 1" copper has a rated working pressure of 655 psig³.

The 0.065 inch wall thickness of type K copper tubing exceeds the minimum required for the 100 psig design pressure.

Stainless steel tubing and pipe is also used in the nitrogen piping. The calculations for minimum wall thickness are the same as the copper calculations shown in the appendix. All copper and stainless steel tubing and pipe used is summarized in Table 2 with the physical property data used in determining the minimum wall thickness.

The amendment does not introduce any new materials or additional pipe/tube sizes.

³ The Copper Tube Handbook, Copper Development Association, A4015-04/06, Table 3a.

Table 2: Minimum Tube / Pipe Wall Thickness

OD (in)	Wall Thk (in)	matl	SA1 (psi)	Ycoef	Wfact.	Efact.	Ea (psi)	Design P (psig)	tmin (in)	wall thk > tmin	note
1.125	0.065	copper, k	6000	0.4	1.0	1.0	1.70E+07	100	0.009	YES	tubing
3.500	0.120	SS	16700	0.4	1.0	1.0	2.83E+07	100	0.010	YES	3" sch 10
1.315	0.109	SS	16700	0.4	1.0	1.0	2.83E+07	100	0.004	YES	1" sch 10
1.000	0.049	SS	16700	0.4	1.0	1.0	2.83E+07	100	0.003	YES	tubing
0.750	0.035	SS	16700	0.4	1.0	1.0	2.83E+07	100	0.002	YES	tubing
0.250	0.035	SS	16700	0.4	1.0	1.0	2.83E+07	100	0.001	YES	tubing

OVER PRESSURE PROTECTION

The liquid nitrogen and liquid argon piping will have trapped volumes, requiring overpressure relief. Fire and thermal overpressure are significant sources of overpressure. The largest relief rate is 43 SCFM air at 110 psig (10% over pressure). Circle-seal 5100 series relief valves with a 4MP orifice provide 54 SCFM at 110 psig (10% over pressure). Details of the pressure relief calculations are in the Appendix 2. No adjustments are made for smaller trapped volumes and the same size relief valve is used. This allows for shared spares and eliminates the risk of error and installation of an undersized relief valve.

The nitrogen vent piping post condenser and post phase separator has no valves or trapped volumes.

The un-insulated $\frac{1}{4}$ inch copper tubing for the nitrogen insulation purges only contains liquid for a short distance until it vaporizes. After that short distance the copper tubing contains only nitrogen gas.

The existing relief valve calculations are valid for the amendment.

6. PIPING STRESS

The supply piping for the nitrogen liquid and gas piping is routed from a FERMLAB LN2 trailer positioned near between PS4 and an electrical substation. The liquid nitrogen piping is routed to a nearby nitrogen vaporizer and over a berm to PC4. The nitrogen gas comes from the nitrogen vaporizer and is also routed over the berm to PC4. The relative position of the trailer, vaporizer and PC4 can be seen in Figure 1.

The specific nitrogen supply pipe routing is documented by the ANSYS FEA flexibility analysis shown in Appendix 3. Piping supports are provided by blocks of plastic that allow the pipes to slide as they contract and expand.

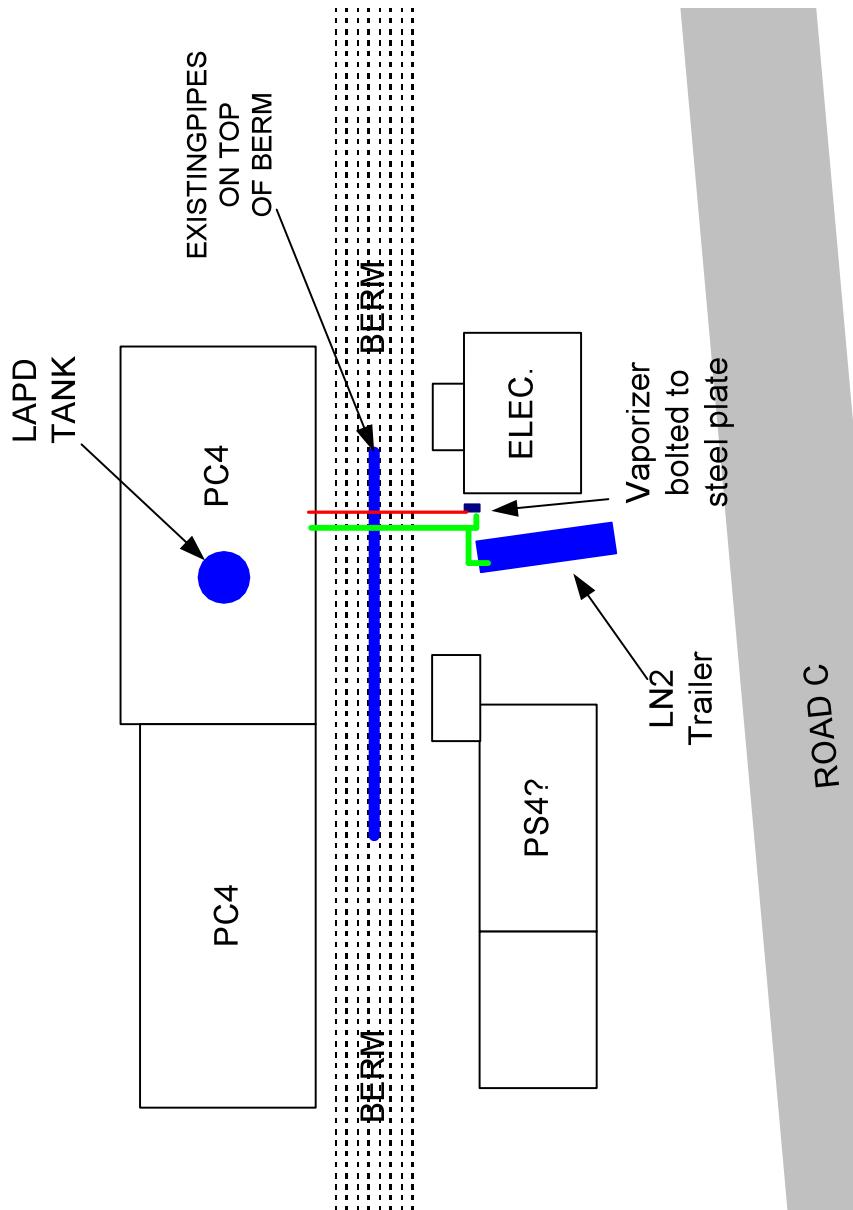
The components added in this amendment do not affect the flexibility of the piping.

All calculated thermal stresses are below the allowable displacement stress range SA as computed by 302.3.5(d):

$$S_A = f(1.25S_c + 0.25S_h) = 1[1.25(6,000) + 0.25(6,000)] = 9,000 \text{ psi}$$

The piping therefore has sufficient flexibility.

Figure 1: N2 SUPPLY PIPING ROUTE



7. CODE REQUIRED DOCUMENTATION

ASME B31.3 requires that the brazing/welding be done by qualified brazers/welders. Brazer/welder qualifications are documented in the appendix.

B31.3 also requires that a representative sampling of the fabrication be inspected, defined as not less than 5% of the fabrication. Inspection forms are available here:

<http://lartpc-docdb.fnal.gov:8080/cgi-bin>ShowDocument?docid=639>

Any inspection forms required by the amendment will be added to the above link.

A leak test is required by B31.3. For the supply piping the test pressure is 110% of design or 110 psig. B31.3 allows for pneumatic testing and pneumatic testing was used. Test results are documented in the Appendix 4.

The required pressure tests for the amendment will be added to Appendix 4.

Appendix 1


Flow Schematics and Valve and Instrument List.


The flow schematic and valve and instrument list are updated for the amendment.

MISC. REVISIONS MADE.

J. CATALANELLO 22-MAY-2012

	J. CATALANELLO	26-FEB-2010	REV	DESCRIPTION	DRAWN	DATE
	M. ADAMOWSKI	26-FEB-2010			APPROVED	DATE
G	J. CATALANELLO	10-JAN-2011	A	ADDED TAG NUMBERS TO VALVE TYPES	V. MAJDANSKI	25FEB08
H	J. CATALANELLO	10-JAN-2011	B	MOVE CONDENSER OUTSIDE TANK	R. SCHMITT	26FEB08
J	J. CATALANELLO	23-FEB-2011	C	MISC. REVISIONS MADE.	J. CATALANELLO	07-DEC-2008
K	J. CATALANELLO	04-MAR-2011	D	MISC. REVISIONS MADE.	R. SCHMITT	10-DEC-2008
L	J. CATALANELLO	22-JUN-2011	E	MISC. REVISIONS MADE.	J. CATALANELLO	06-JAN-2009
	J. CATALANELLO	11-JUL-2011		MISC. REVISIONS MADE.	J. CATALANELLO	17-NOV-2009
	T. TOPE	01-MAR-2012		MISC. REVISIONS MADE.	T. TOPE	14-DEC-2009
	J. CATALANELLO				J. CATALANELLO	15-JAN-2010
	T. TOPE				T. TOPE	






UNLESS OTHERWISE SPECIFIED ORIGINATOR R.SCHMITT 26-JUN-2007
DRAWN J.CATALANELLO 07-DEC-2007
CHECKED R.SCHMITT 12-DEC-2007
APPROVED R.SCHMITT 12-DEC-2007
USED ON
MATERIAL

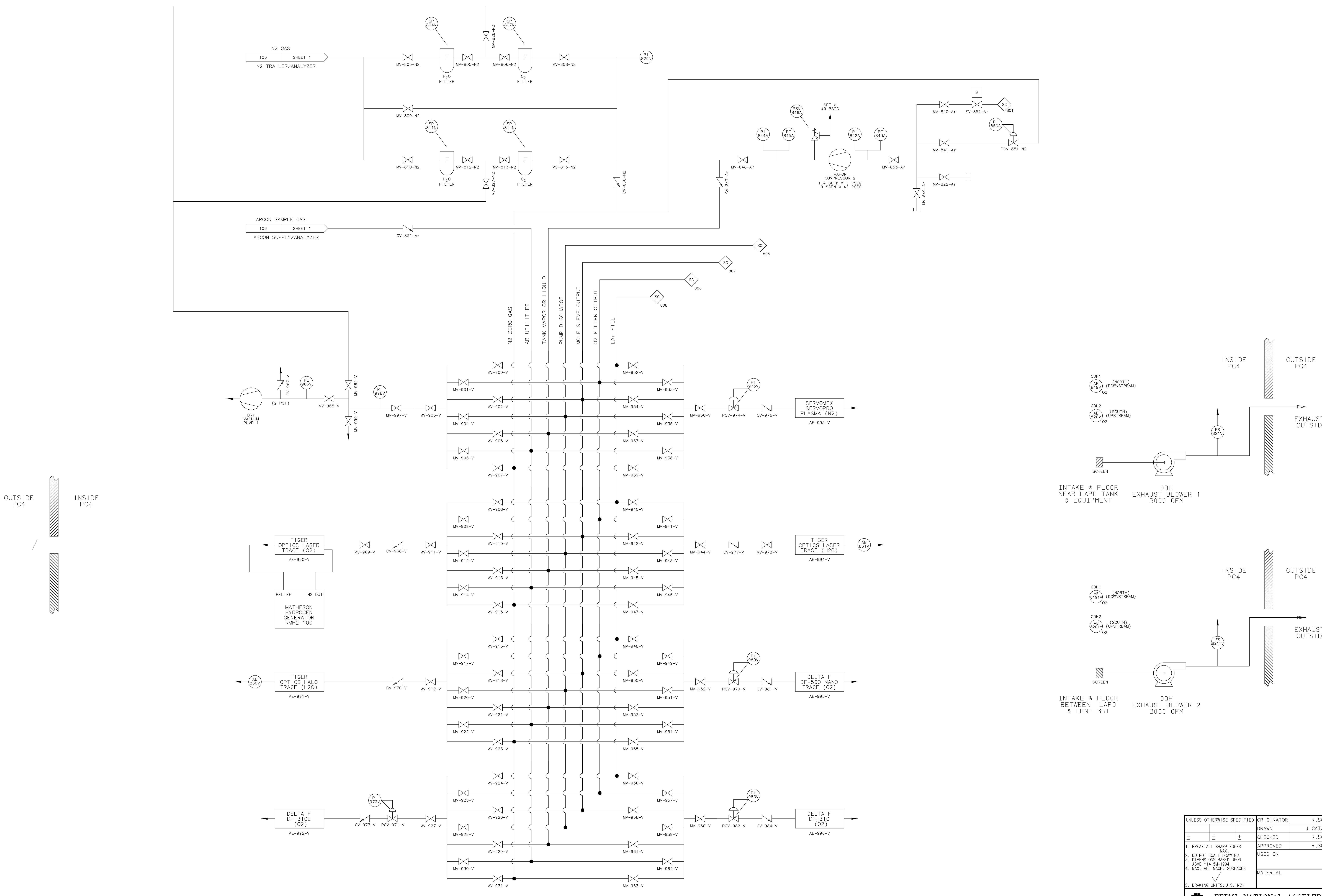
1. BREAK ALL SHARP EDGES
MAX.
2. DO NOT SCALE DRAWING
DIMENSIONS ARE IN U.S. INCHES
3. DRAWING BASED UPON
ASME Y14.5M-1994
4. MAX. AL MACH. SURFACES
5. DRAWING UNITS: U.S. INCH

FERMI NATIONAL ACCELERATOR LABORATORY
UNITED STATES DEPARTMENT OF ENERGY
FLARE UTILITIES
GAS PIPING & INSTRUMENT DIAGRAM
LIQUID ARGON PURITY DEMONSTRATION

SCALE DRAWING NUMBER 3942.510-ME-444897 SHEET 2 OF 4 REV M
NONE

CREATED WITH : Ideas12NXSeries GROUP: PPD/MECHANICAL DEPARTMENT





UNLESS OTHERWISE SPECIFIED	ORIGINATOR	R. SCHMITT	26-JUN-2007
DRAWN	J. CATALANELLO	07-DEC-2007	
+	+	+	
CHECKED	R. SCHMITT	12-DEC-2007	
APPROVED	R. SCHMITT	12-DEC-2007	
USED ON			
MATERIAL			
5. DRAWING UNITS: U.S. INCH			

FERMI NATIONAL ACCELERATOR LABORATORY
UNITED STATES DEPARTMENT OF ENERGY

FLARE UTILITIES
GAS PIPING & INSTRUMENT DIAGRAM
L I Q U I D A R G O N P U R I T Y D E M O N S T R A T I O N

SCALE	DRAWING NUMBER	SHEET	REV
NONE	3942.510-ME-444897	4	4

CREATED WITH : iIdeas12NXSeries GROUP: PPD/MECHANICAL DEPARTMENT

Instr Code	Tag #	Serv. Code	PID	SD G	LC	Service Description	Instrument Type	Operating Range or Setpoint	Pressure Rating	Manufacturer	Model No.
CV	977	V	SHT-4	-4-	C	gas analyzers	check valve	2 psig	3000 psig	Swagelok	6L-CW4FR4
MV	978	V	SHT-4	-4-	C	gas analyzers	manual valve	NA	375 psig	Carten	MD-250
PCV	979	V	SHT-4	-4-	C	gas analyzers	pressure control valve	0 - 30 psig	300 psig	Matheson	9332-3-V4FF
PI	980	V	SHT-4	-4-	C	gas analyzers	pressure indicator	30"-0-60 psig	60 psig	Matheson	supplied with regulator
CV	981	V	SHT-4	-4-	C	gas analyzers	check valve	2 psig	3000 psig	Swagelok	6L-CW4FR4
PCV	982	V	SHT-4	-4-	B	gas analyzers	pressure control valve	0 - 30 psig	300 psig	Matheson	9332-3-V4FF
PI	983	V	SHT-4	-4-	B	gas analyzers	pressure indicator	30"-0-60 psig	60 psig	Matheson	supplied with regulator
CV	984	V	SHT-4	-4-	B	gas analyzers	check valve	2 psig	3000 psig	Swagelok	6L-CW4FR4
AE	990	V	SHT-4	-7-	D	gas analyzers	oxygen analyzer	0 - 2.5 ppm	125 psig	Tiger Optics	LaserTrace H2O
AE	991	V	SHT-4	-7-	C	gas analyzers	water analyzer	0 - 20 ppm	125 psig	Tiger Optics	Halotrace H2O
AE	992	V	SHT-4	-7-	B	gas analyzers	oxygen analyzer	0 - 50 ppm	30 psig	Delta-F	DF-310E
AE	993	V	SHT-4	-4-	D	gas analyzers	nitrogen analyzer	0 - 100 ppm	30 psig	Servomex/Kontrol Analytik	K2001
AE	994	V	SHT-4	-4-	D	gas analyzers	water analyzer	0 - 5 ppm	125 psig	Tiger Optics	LaserTrace H2O
AE	995	V	SHT-4	-4-	B	gas analyzers	oxygen analyzer	0 - 100 ppm	30 psig	Delta-F	NanoTrace II DF-560
AE	996	V	SHT-4	-4-	A	gas analyzers	oxygen analyzer	0 - 5000 ppm	30 psig	Delta-F	DF-310
MV	997	V	SHT-4	-6-	E	gas analyzers	manual valve	NA	375 psig	Carten	MD-250
PI	998	V	SHT-4	-6-	E	gas analyzers	pressure indicator	vac - 60 psig	60 psig	Wika	230.15-B-PV352-Z-WI-UZ-ZZZ ZZ
MV	999	V	SHT-4	-6-	D	gas analyzers	manual valve	NA	375 psig	Carten	MD-250
SP	1001	N2	SHT-1	-3-	G	N2 liquid to LBNE 35T	particulate filter	NA	1400 psig	McMaster	4745K555
MV	1002	N2	SHT-1	-3-	G	N2 liquid to LBNE 35T instrumentation	manual valve	NA	1000 psig	Swagelok	B-4HK2
MV	1003	N2	SHT-1	-3-	G	N2 liquid to LBNE 35T instrumentation	manual valve	NA	1000 psig	Swagelok	B-4HK2
PI	1004	N2	SHT-1	-3-	G	N2 liquid to LBNE 35T instrumentation	pressure indicator	vac - 150 psig	150 psig	US Gauge	FNAL STK 1050-003500
MV	1005	N2	SHT-1	-3-	G	N2 liquid to LBNE 35T	manual valve	NA	870 psig	Worcester	1" #C4466 PM SW
MV	1006	N2	SHT-1	-3-	G	N2 liquid to LBNE 35T instrumentation	manual valve	NA	1000 psig	Swagelok	B-4HK2
MV	1007	N2	SHT-1	-3-	G	N2 liquid to LBNE 35T instrumentation	manual valve	NA	1000 psig	Swagelok	B-4HK2
PSV	1008	N2	SHT-1	-3-	G	N2 liquid to LBNE 35T	relief valve	100 psig	2400 psig	Circle Seal	5100-4MP
PI	1009	N2	SHT-1	-3-	G	N2 liquid to LBNE 35T instrumentation	pressure gauge	vac - 150 psig	150 psig	US Gauge	FNAL STK 1050-003500
PT	1010	N2	SHT-1	-3-	G	N2 liquid to LBNE 35T	pressure transmitter	vac - 135 psig	135 psig	Setra	5161-135P-C-2M-11-B1-H
MV	5001	Ar	SHT-3	-4-	A	LBNE 35T to filter (isolation)	manual valve	NA	165 psid	Eden Cryogenics	BC-02146-8101
MV	5002	Ar	SHT-3	-7-	F	LBNE 35T from filters (isolation)	manual valve	NA	165 psid	Eden Cryogenics	BC-02146-8101

Appendix 2

MathCad Wall Thickness, Trapped Volume Relief Sizing, and Ambient Vaporizer Wind Loading Calculations

LAPD N2 Supply Piping Min Wall Thickness

rev. 09-06-10

The minimum thickness of the piping is dictated by ASME B31.3, 304.1.2(a), Straight Pipe Under Internal Pressure.

The solenoids used for the nitrogen service can operate up to a maximum pressure differential of 100 psig. The 100 psig will be used as the design pressure.

Piping/Tubing Design Gage Pressure

$$P_{\text{design}} := 100 \cdot \text{psi} \quad g$$

LN2 Density @100 psig per refprop

$$\text{LN2}_{\text{dens}} := 50.5 \cdot \frac{\text{lbf}}{\text{ft}^3}$$

Basic Brazed (Socket) Copper Tubing Data

Allowable Copper Tubing Stress, Table A-1

$$S_{A1} := 6000 \cdot \text{psi}$$

ref: ASME B31.3-2008

SIF, stress intensification factor,
B31.3 Table D300, note (13)

$$\text{SIF} := 2.1$$

Y coefficient from B31.3, Table 304.1.1

$$Y_{\text{coeff}} := 0.4$$

Weld strength reduction factor, B31.3,
302.3.5(e)

$$W_{\text{factor}} := 1.00$$

Quality factor, Table A-1B

$$E_{\text{factor}} := 1.00$$

reference modulus of elasticity at 70 F,
Table C-6

$$E_a := 17 \cdot 10^6 \cdot \text{psi}$$

Tubing Data, Type K Copper Tubing

The largest copper tube size used is 1". Smaller 3/4" and 1/2" tubing is also used.

Nominal Tube Wall Thickness	Tube Outside Diameter	
$T_{Wall,1} : = 0.065 \cdot \text{in}$	$Tube_{OD,1} : = 1.125 \cdot \text{in}$	ref: The Copper Tube Handbook, Copper Development Association, A4015-04/06, Table 2a.
$T_{Wall,3Q} : = 0.065 \cdot \text{in}$	$Tube_{OD,3Q} : = 0.875 \cdot \text{in}$	
$T_{Wall,half} : = 0.049 \cdot \text{in}$	$Tube_{OD,half} : = 0.625 \cdot \text{in}$	

Minimum Wall Thickness

per B31.3-2008 eqn 3.

$$\frac{Tube_{OD,1}}{6} = 0.188 \cdot \text{in}$$

wall thickness of the largest tube size is less than D/6 therefore B31.3, equation 3a applies.

For 1" tubing

$$t_{min,req,1} : = \frac{P_{design} \cdot Tube_{OD,1}}{2 \cdot (S_{A1} \cdot E_{factor} \cdot W_{factor} + P_{design} \cdot Y_{coeff})} = 0.0093 \cdot \text{in}$$

actual tube wall thickness $T_{Wall,1} = 0.065 \cdot \text{in}$

For 3/4" tubing

The 3/4" tubing has the same wall thickness as the 1" tubing. B31.3 minimum wall thickness goes down with decreasing diameter. Therefore the 3/4" tube wall also exceeds the minimum required.

For 1/2" tubing

$$t_{min,req,half} : = \frac{P_{design} \cdot Tube_{OD,half}}{2 \cdot (S_{A1} \cdot E_{factor} \cdot W_{factor} + P_{design} \cdot Y_{coeff})} = 0.0052 \cdot \text{in}$$

actual tube wall thickness $T_{Wall,half} = 0.049 \cdot \text{in}$

Actual wall thickness exceeds the minimum wall thickness called for by B31.3 for the 1", 3/4" and 1/2" type K copper tubing selected.

N2 Supply Piping Trapped Volume Relief Sizing

This calculation is for sizing the relief rate for trapped volumes in the LN2 supply piping for LAPD. The formulas and factors are per CGA S-1.3-2005, piping pressure relief.

The outdoor piping will pass over a grassy berm. Since the grass is flammable, fire case is evaluated with part of the pipe exposed to fire. It is assumed that that a 10 ft section of pipe could be exposed to fire.

There are no flammables that could engulf the pipe and LN2 is not flammable so the required relief capacity will be reduced to 30% of calculated as allowed for in CGA S-1.3-2005, section 6.3.

The LN2 piping is pre-insulated in polyurathane with a PVC jacket.

Fire Relief

Pipe outside diameter, 1" copper	Pipe Length	Total Outside Pipe Surface Area
$\text{Pipe}_{\text{dia}} := \text{Tube}_{\text{OD},1} = 1.125 \cdot \text{in}$	$\text{Pipe}_{\text{l,fir}} := 10 \cdot \text{ft}$	$\text{Area}_{\text{pipe}} := 2\pi \frac{\text{Pipe}_{\text{dia}}}{2} \cdot \text{Pipe}_{\text{l,fir}}$ $\text{Area}_{\text{pipe}} = 2.9 \cdot \text{ft}^2$

Area for CGA formula, converted into unitless value from Area in ft²

$$A := \frac{\text{Area}_{\text{pipe}}}{\text{ft}^2} = 2.9$$

N2 Uninsulated Gas Factor, CGA S-1.3-2005, Table 1

$G_U := 59.0$ @ min working pressure of 100 psig

CGA S-1.3-2005 has a error in Table 1 where the data is shifted. The correct value is used here and verified from the 2008 version.

Correction Factor per CGA S-1.3-2005, sec. 6.1.4
(inlet to RV is less than 2 ft so correction factor is 1)

$F := 1$

Required CGA Fire Relief Rate (sec 6.3.2)

$$Q_{\text{a,fir}} := 30\% F \cdot G_U \cdot A^{0.82} \cdot \frac{\text{ft}^3}{\text{min}} = 42.9 \cdot \frac{\text{ft}^3}{\text{min}} \quad \text{SCFM air @ 60 F (cap. at 21% overpres.)}$$

Relief size check for other than fire

Pipe outside diameter	Insulation outside diameter	Arithmetic mean of surface diameters
Pipe _{dia} = 1.125·in	Insul _{dia} : = 6·in	Avg _{dia} : = $\frac{(Pipe_{dia} + Insul_{dia})}{2}$ = 3.6·in
Relief T	Pipe Length	Area based on arithmetic mean surface diameter
T : = -320 °F	Pipe _{l.sect} : = 200·ft	Area : = $2\pi \frac{Avg_{dia}}{2} \cdot Pipe_{l.sect}$ Area = 186.5·ft ²

Area for CGA formula, converted into unitless value from Area in ft²

$$A : = \frac{\text{Area}}{\text{ft}^2} = 186.5$$

Insulation thickness

$$Insul_{thick} : = \frac{(Insul_{dia} - Pipe_{dia})}{2} = 2.4 \cdot \text{in}$$

N2 Uninsulated Gas Factor, CGA S-1.3-2005, Table 1

$$G_i : = 10.2 \quad @ \text{ min working pressure of } 100 \text{ psig}$$

CGA S-1.3-2005 has a error in Table 1 where the data is shifted. The correct value is used here and verified from the 2008 version.

Insulation thermal conductivity

$$k : = 0.5 \cdot \frac{\text{BTU} \cdot \text{in}}{\text{hr} \cdot \text{ft}^2 \cdot \text{F}}$$

Overall U based on

$$U_{insul} : = \frac{k}{Insul_{thick}} = 0.2 \cdot \frac{\text{BTU}}{\text{hr} \cdot \text{ft}^2 \cdot \text{F}}$$

$$U : = \frac{U_{insul}}{\frac{\text{BTU}}{\text{hr} \cdot \text{ft}^2 \cdot \text{F}}} = 0.2 \quad \begin{matrix} \text{make} \\ \text{unitless} \\ \text{U for} \\ \text{CGA} \\ \text{formula} \end{matrix}$$

Correction Factor per CGA S-1.3-2005, sec. 6.1.4
(inlet to RV is less than 2 ft so correction factor is 1)

$$F : = 1$$

Required CGA Thermal Heating (non-fire) Relief Rate (sec 6.2.2)

$$Q_a : = \frac{[590 - (T + 459.67)]}{4 \cdot [1660 - (T + 459.67)]} \cdot F \cdot G_i \cdot U \cdot A \cdot \frac{\text{ft}^3}{\text{min}} = 28.9 \cdot \frac{\text{ft}^3}{\text{min}}$$

SCFM air @ 60 F (cap. at 10% overpres.)

$$Q_{a.\text{fire}} = 42.9 \cdot \frac{\text{ft}^3}{\text{min}} \text{ SCFM air @ 60 F (cap. at 21% overpres.)}$$

The thermal heating scenario is the larger rate and this rate will be used in selecting the relief device. Use of this rate for shorter lengths of the same or smaller diameter insulated pipe would be conservative.

From the Circle Seal line of relief valves, the 4MP size will be used. The 4MP

Air Flow Rates (5100-MP)

Inline valves, $\frac{1}{8}$ "–1"

Crack Pressure PSIG	Percent Over Pressure Beyond Cracking (SCFM air at room temperature)						
	10%				25%		
	1MP	2MP/3MP	4MP	6MP/8MP	1MP	2MP/3MP	4MP
15	1.0	1.5	5.0	9.0	3.0	5.0	50
20	1.5	2.0	10	12	4.0	5.0	60
25	2.0	2.7	25	27	5.4	6.5	65
30	2.4	4.6	30	36	6.2	13	68
40	3.0	5.5	34	55	6.5	25	72
50	3.0	10.5	40	65	8.0	29	74
75	4.2	14	50	70	13	38	80
100	6.0	25	54	90	17	55	90
125	8.5	32	70	120	22	58	110
150	10	36	72	150	27	78	115

N2 Ambient Vaporizer Wind Load

The LAPD N2 ambient vaporizer will be bolted to a steel plate as part of the temporary N2 supply system to LAPD. This calculation determines the additional weight needed to keep the vaporizer from tipping over in a gust of wind.

Vaporizer Data:

Vaporizer Largest Profile Area

$$V_{\text{area}} : = (45 \cdot \text{in} - 3 \cdot 4 \cdot \text{in}) \cdot 120 \cdot \text{in} = 27.5 \cdot \text{ft}^2$$

The largest profile area is the widest side minus the three open space between fins.

Vaporizer Empty Weight

$$V_{\text{wt}} : = 275 \cdot \text{lb}$$

Ballast in form of plate and additional weights

$$\text{ballast} : = 700 \cdot \text{lb} \quad \text{approx. } 5 \text{ ft} \times 7 \text{ ft} \times 0.5 \text{ in steel plate}$$

The vaporizer is treated as a simple vertical structure against a horizontal wind against the largest flat profile.

Basic Wind Speed, ASCE 7-05, Fig 6-1

$$W_{\text{speed,basic}} : = 90 \cdot \text{mph}$$

per ASCE 7-05, Minimum Design Loads for Buildings and Other Structures.

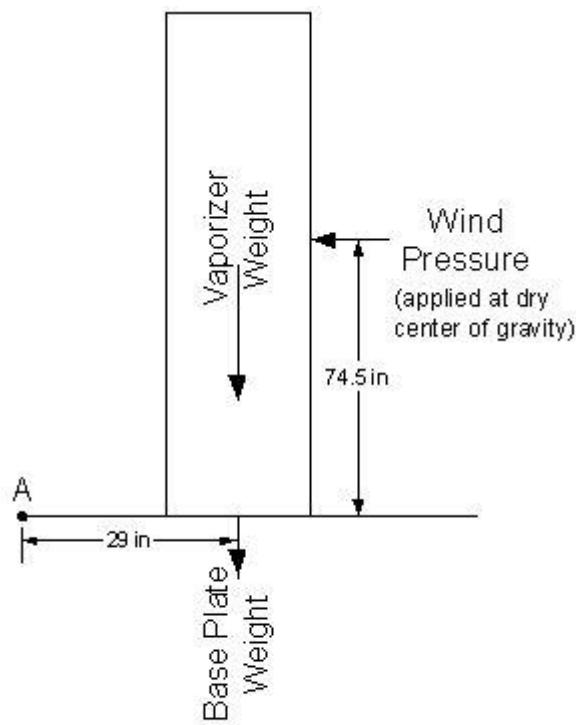
Minimum Wind Design Pressure for above basic wind speed, ASCE 7-05, Fig 6-2

$$P_{\text{wind}} : = 12.8 \cdot \frac{\text{lbf}}{\text{ft}^2}$$

Wind Load on side with largest profile

$$\text{Wind}_{\text{load}} := V_{\text{area}} \cdot \frac{P_{\text{wind}}}{g} = 352 \cdot \text{lb}$$

The moments around the edge of the plate, point A, are calculated counter clockwise per the vaporizer figure shown.



$$\text{Moment}_A := \text{Wind}_{\text{load}} \cdot (74.5 \cdot \text{in}) - (V_{\text{wt}} \cdot 29 \cdot \text{in}) - (\text{ballast} \cdot 29 \cdot \text{in})$$

$$\text{Moment}_A = -172.7 \cdot \text{lb} \cdot \text{ft}$$

The total of moments is negative, indicating that the wind load is insufficient to tip over the empty vaporizer.

The resistance to tipping increases when the vaporizer is used due to the additional weight of LN₂ and ice.

Appendix 3

ANSYS Flexibility Analysis

Figure A3.1: LN2 Supply Piping FEA Model Details

ANSYS

JUL 12 2011
21:00:27
PLOT NO. 1

1 ELEMENTS

MAT NUM

XYZ constrained at horizontal support to limit movement at the phase separator.

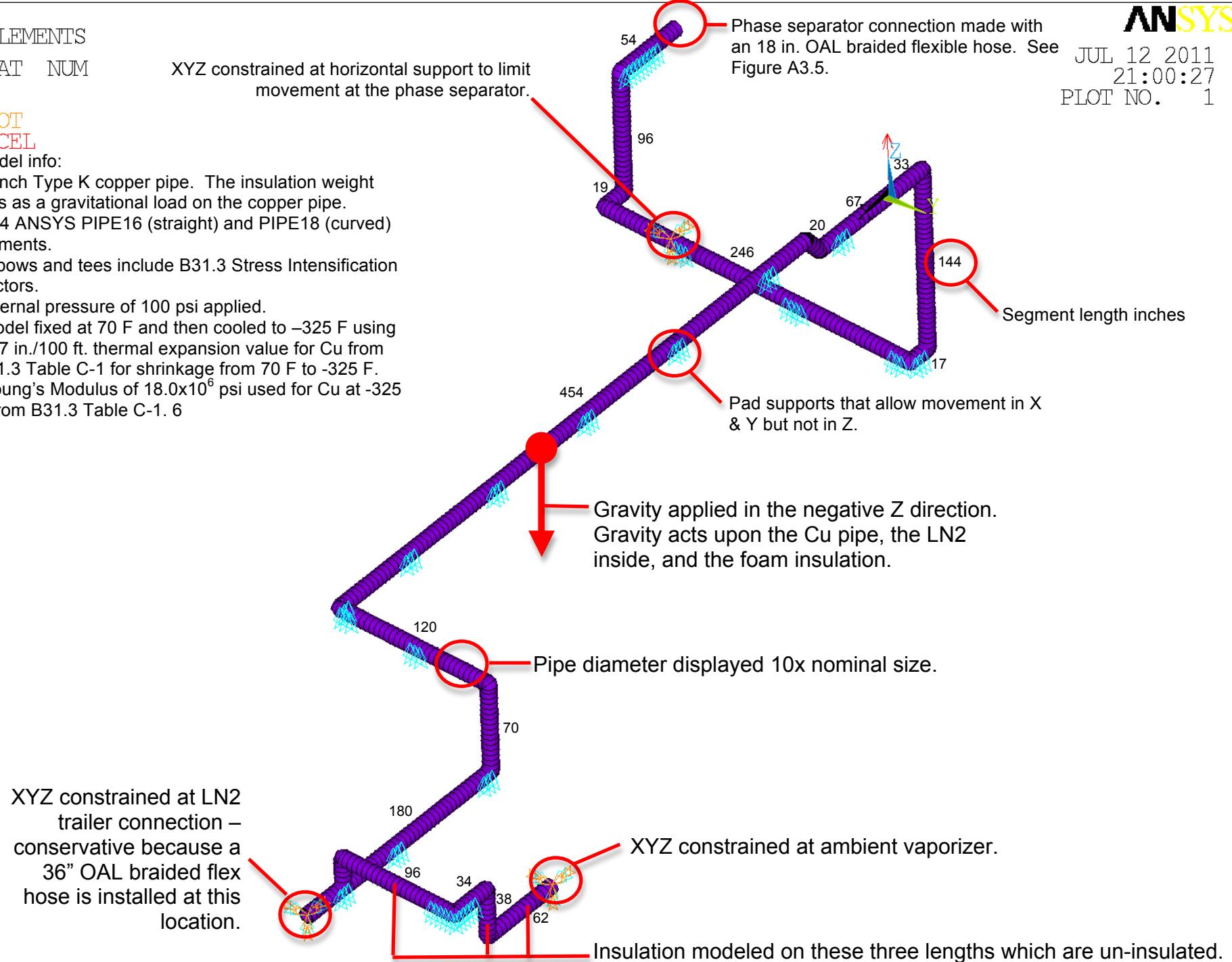
U

ROT

ACEL

Model info:

- 1 inch Type K copper pipe. The insulation weight acts as a gravitational load on the copper pipe.
- 504 ANSYS PIPE16 (straight) and PIPE18 (curved) elements.
- Elbows and tees include B31.3 Stress Intensification Factors.
- Internal pressure of 100 psi applied.
- Model fixed at 70 F and then cooled to -325 F using 3.67 in./100 ft. thermal expansion value for Cu from B31.3 Table C-1 for shrinkage from 70 F to -325 F.
- Young's Modulus of 18.0×10^6 psi used for Cu at -325 F from B31.3 Table C-1. 6



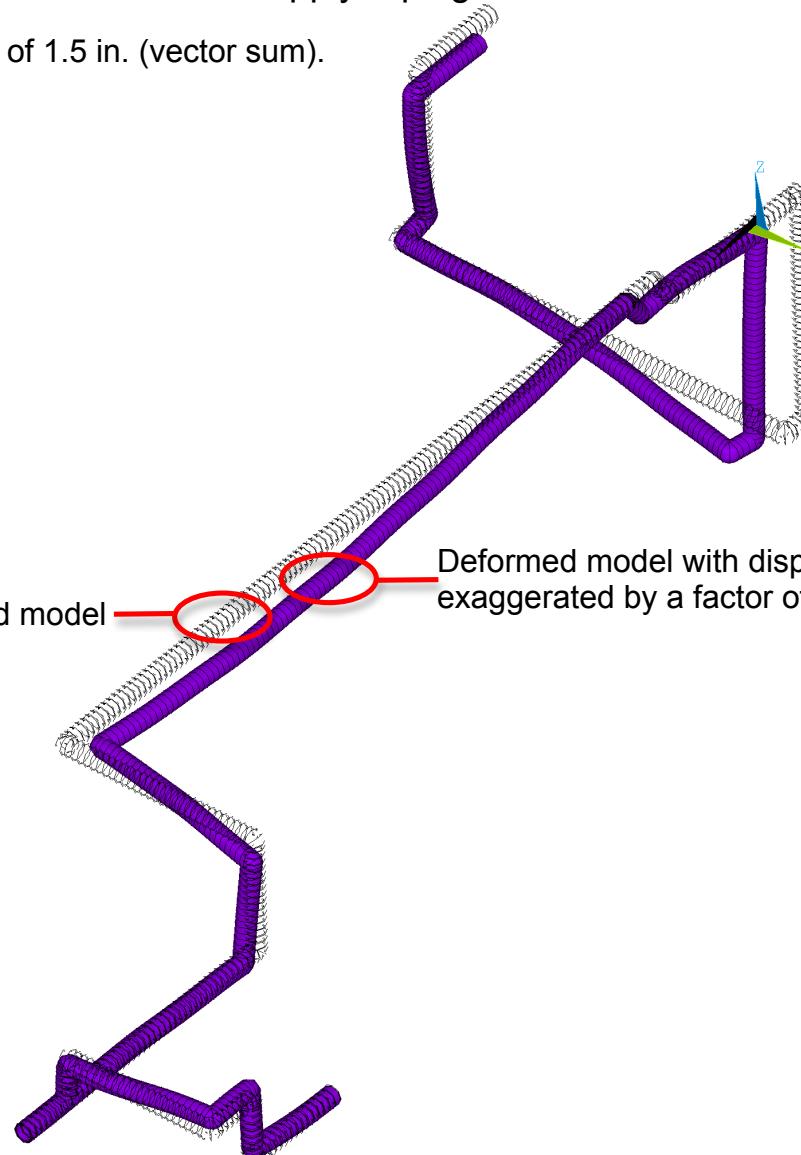
1
DISPLACEMENT
STEP=1
SUB =1
TIME=1
DX =1.496

Figure A3.2: LN2 Supply Piping FEA Deformed Shape

ANSYS
JUL 12 2011
20:59:24
PLOT NO. 1

Maximum displacement of 1.5 in. (vector sum).

Un-deformed model Deformed model with displacements exaggerated by a factor of 20.



NODAL SOLUTION
STEP=1
SUB =1
TIME=1
USUM (AVG)
RSYS=0
DMX =1.496
SMX =1.496

Figure A3.3: LN2 Supply Piping FEA Displacement Contours

ANSYS
JUL 12 2011
20:58:29
PLOT NO. 1

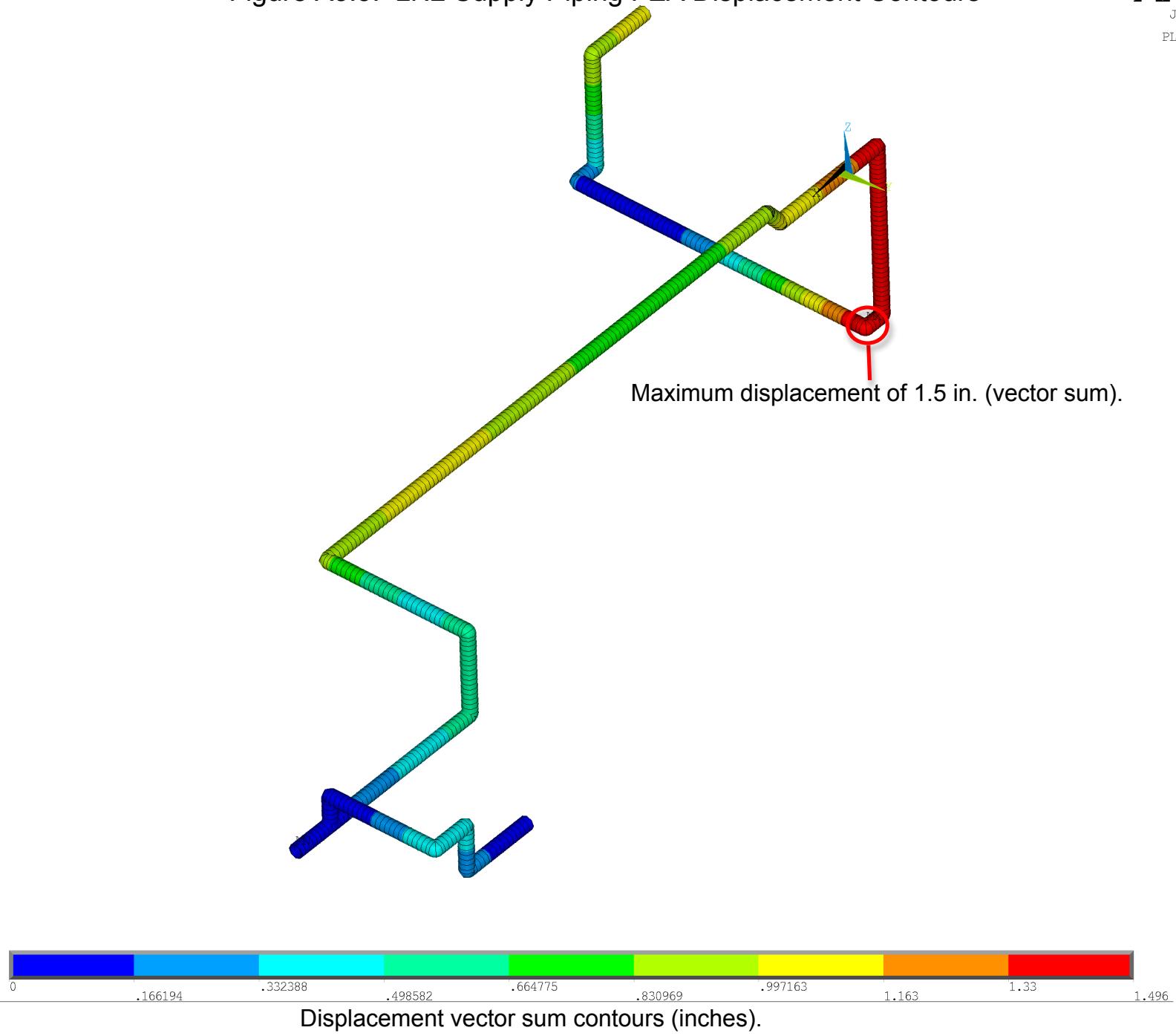


Figure A3.4: LN2 Supply Piping FEA Von Mises Stress Contours

1
NODAL SOLUTION
STEP=1
SUB =1
TIME=1
SEQV (AVG)
DMX =1,496
SMN =622,197
SMX =5985

ANSYS
JUL 12 2011
20:57:50
PLOT NO. 1

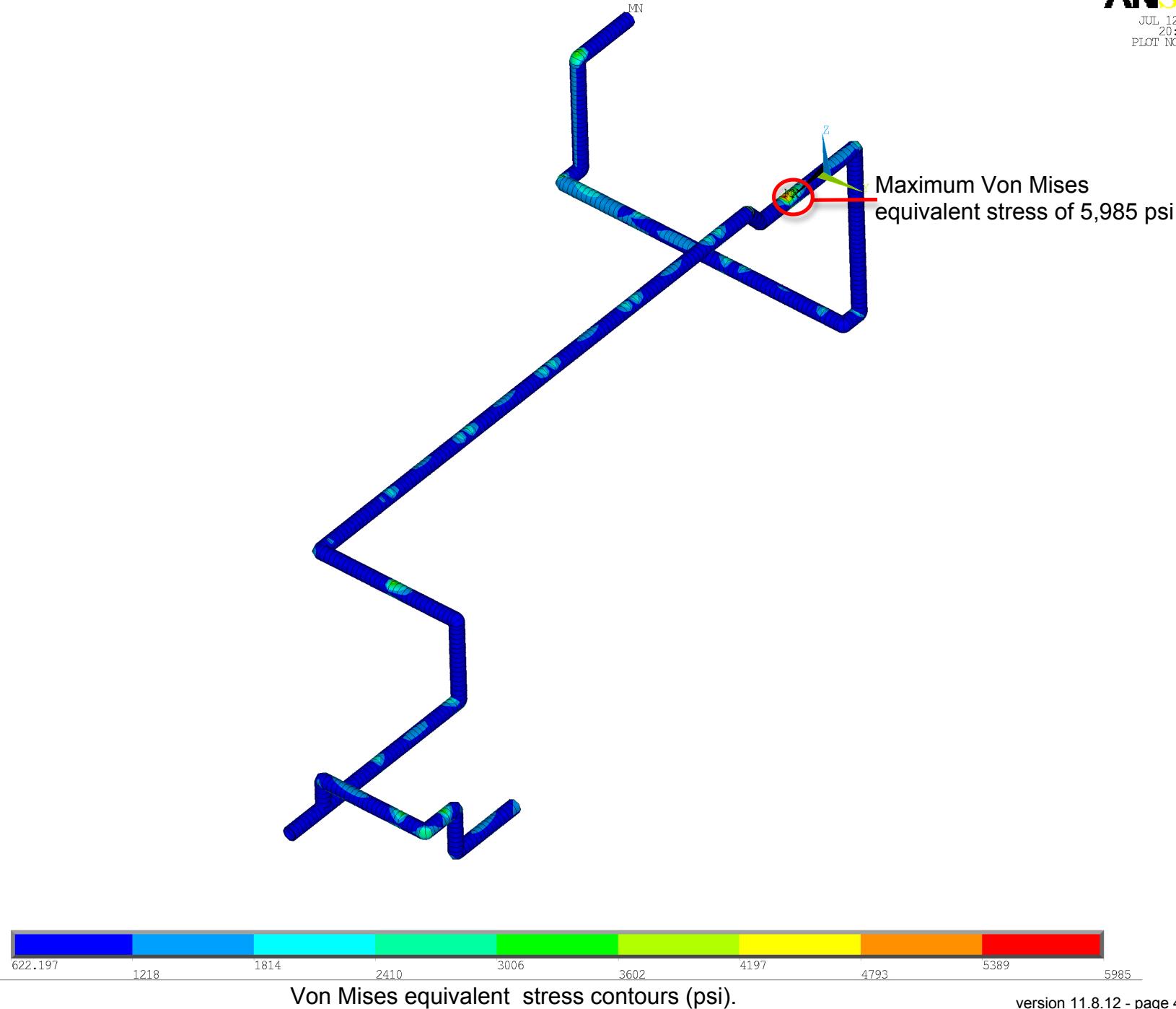


Figure A3.5: LN2 Supply Piping Phase Separator and Condenser View (side)

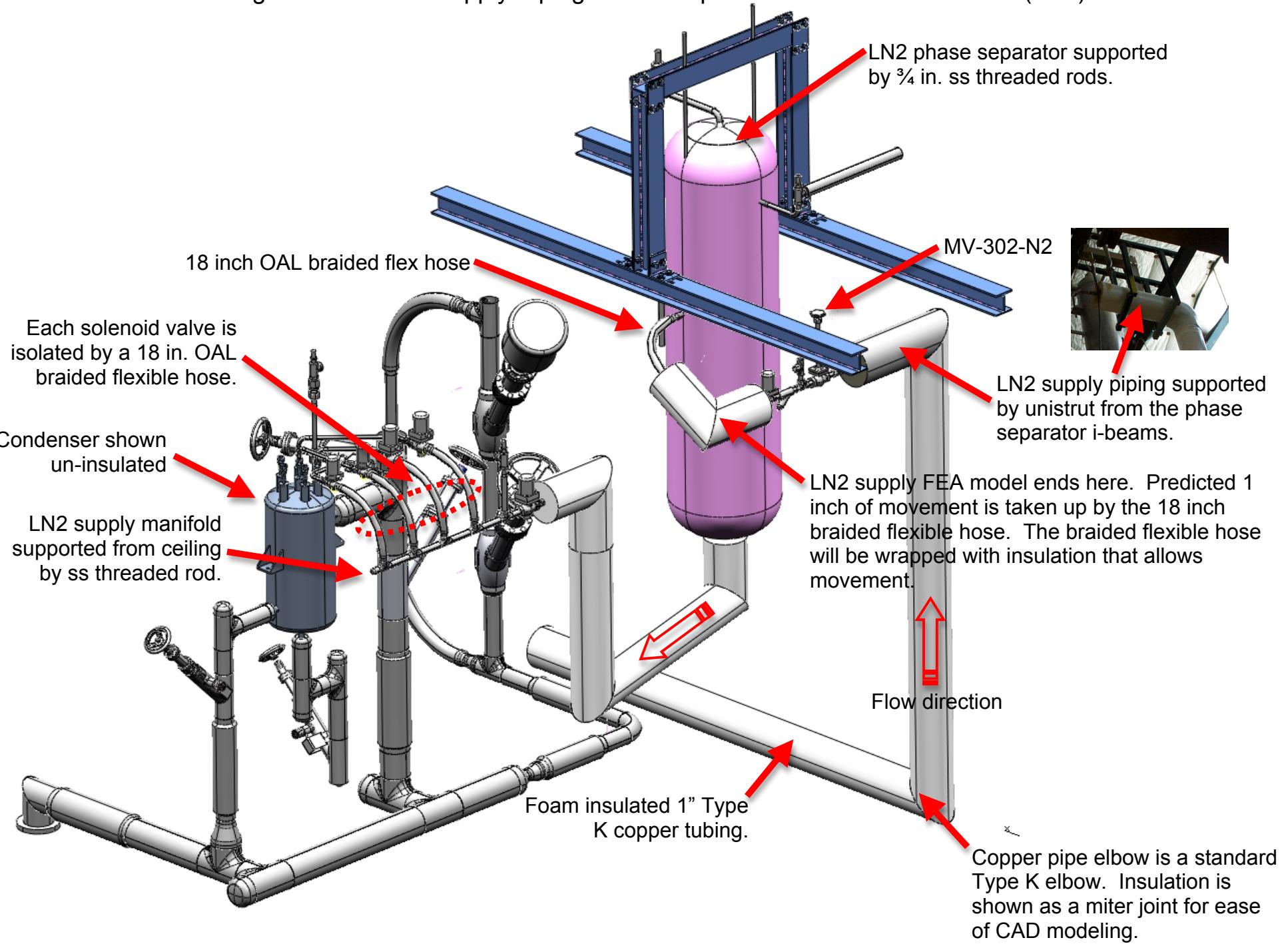


Figure A3.6: LN2 Supply Piping Phase Separator and Condenser View (top)

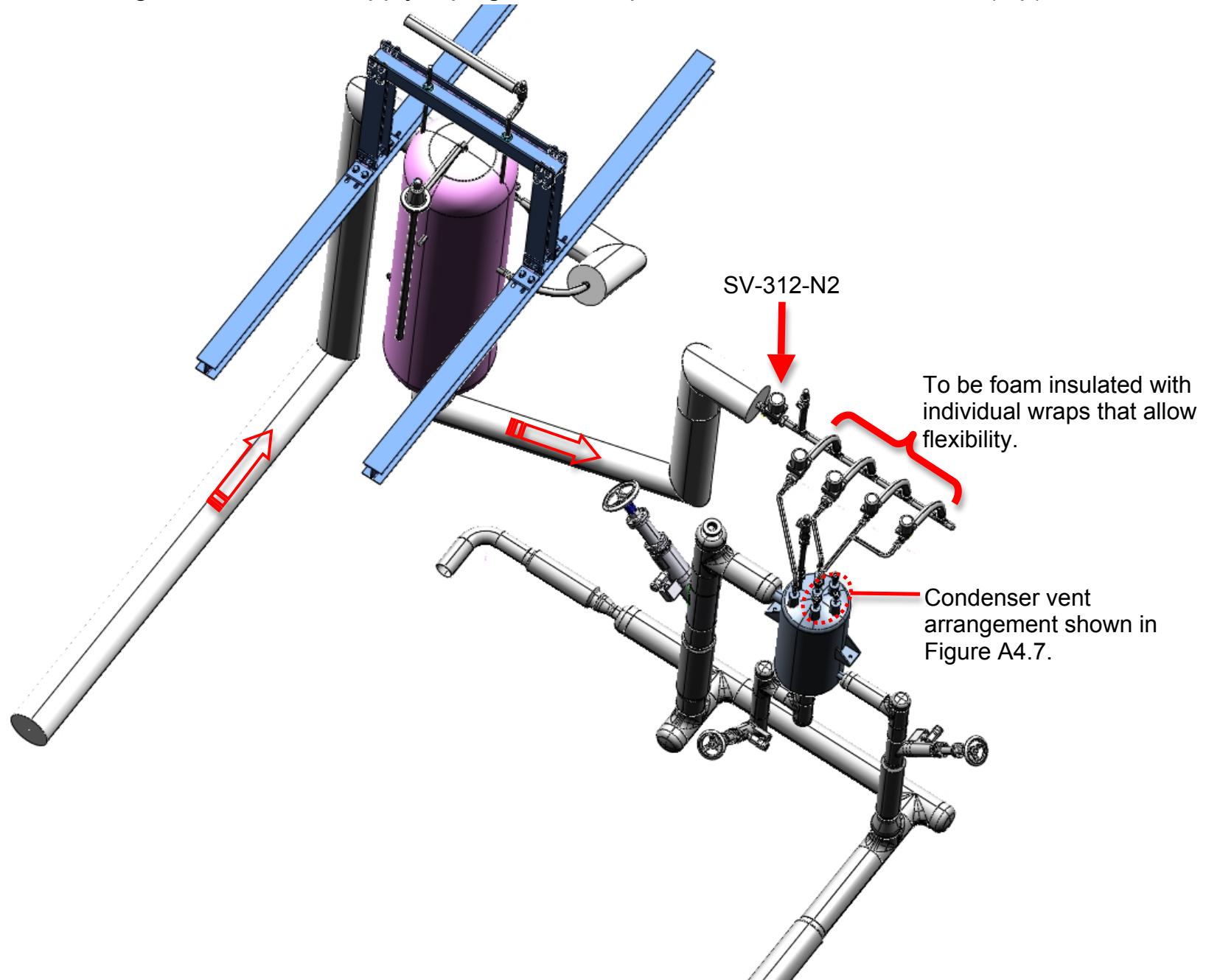
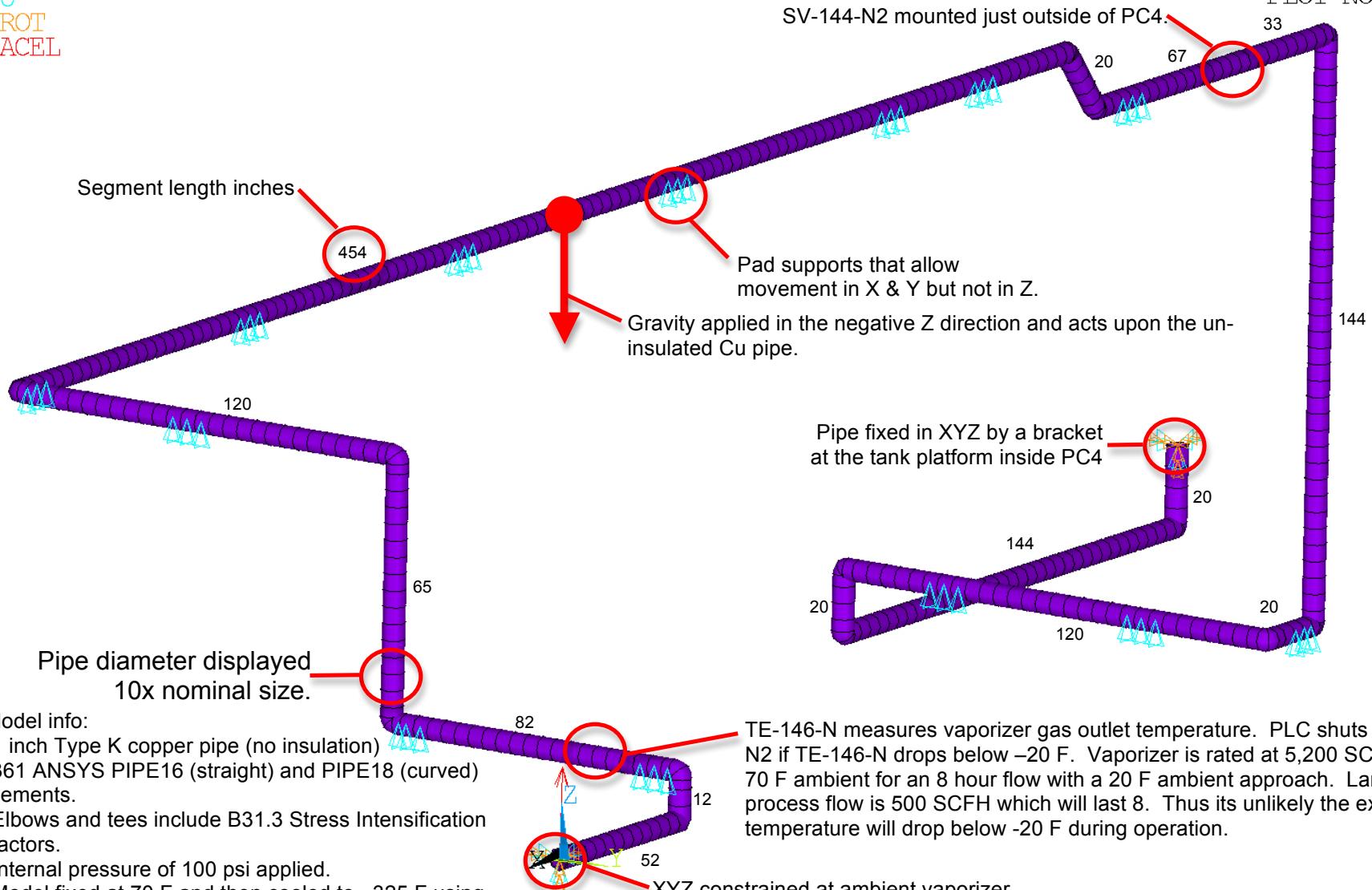


Figure A3.7: Condenser Vent Arrangement



1 ELEMENTS
MAT NUM
U ROT
ACEL

Figure A3.8: GN2 Supply Piping FEA Model Details



GN2_side_v4.db

Figure A3.9: GN2 Supply Piping FEA Deformed Shape

DISPLACEMENT
STEP=1
SUB =1
TIME=1
DMX =1.751

Maximum displacement of 1.75 in. (vector sum).

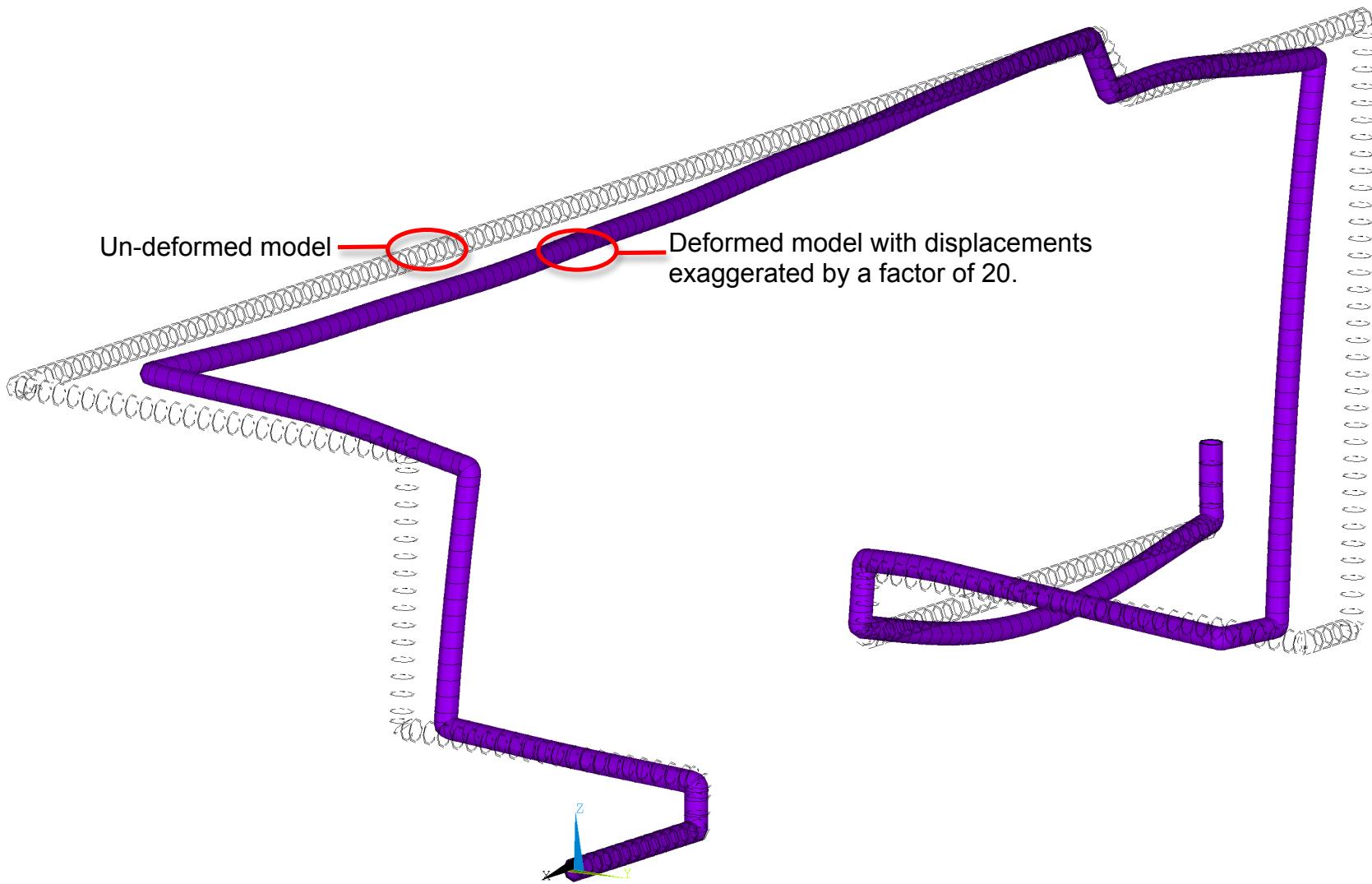
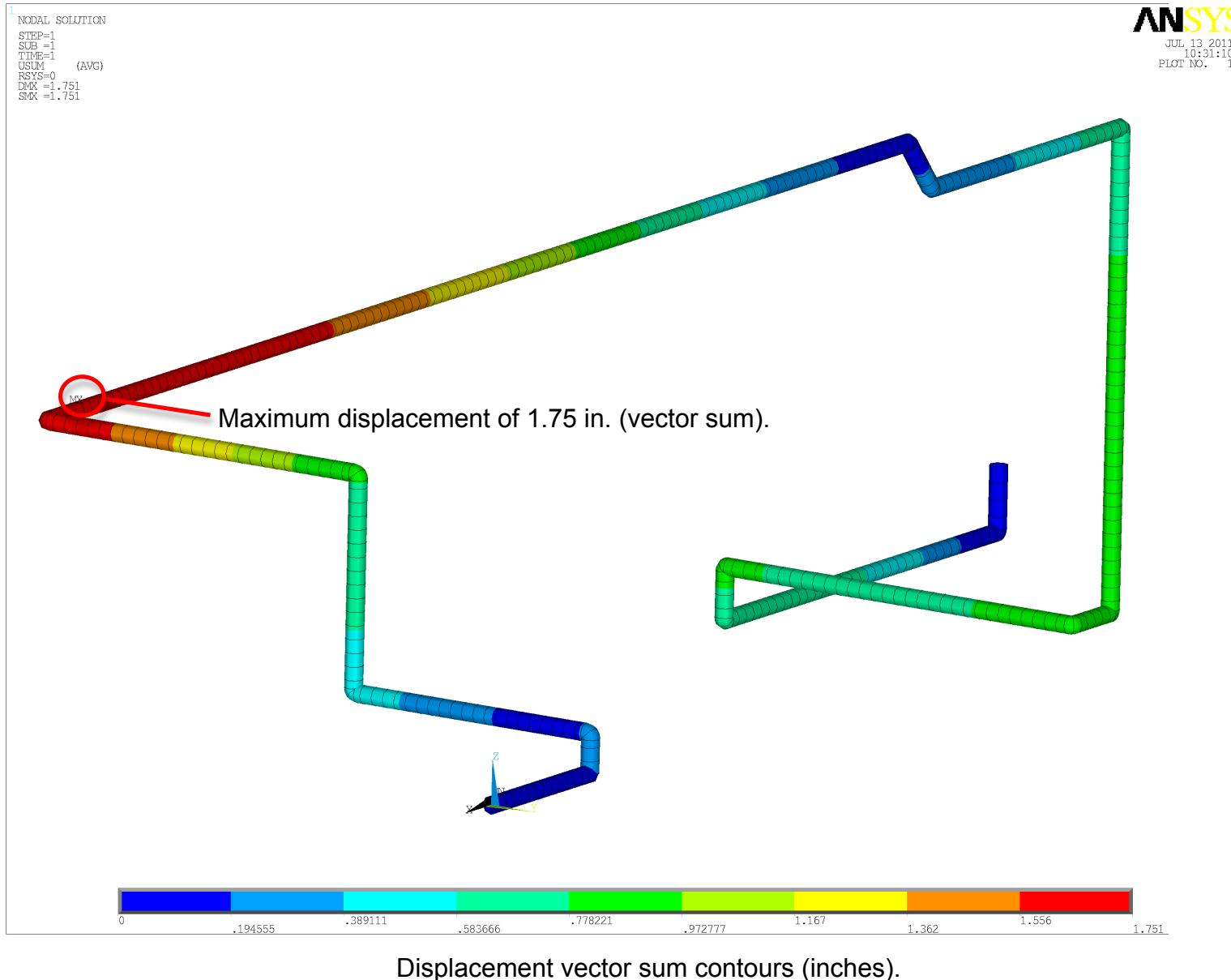


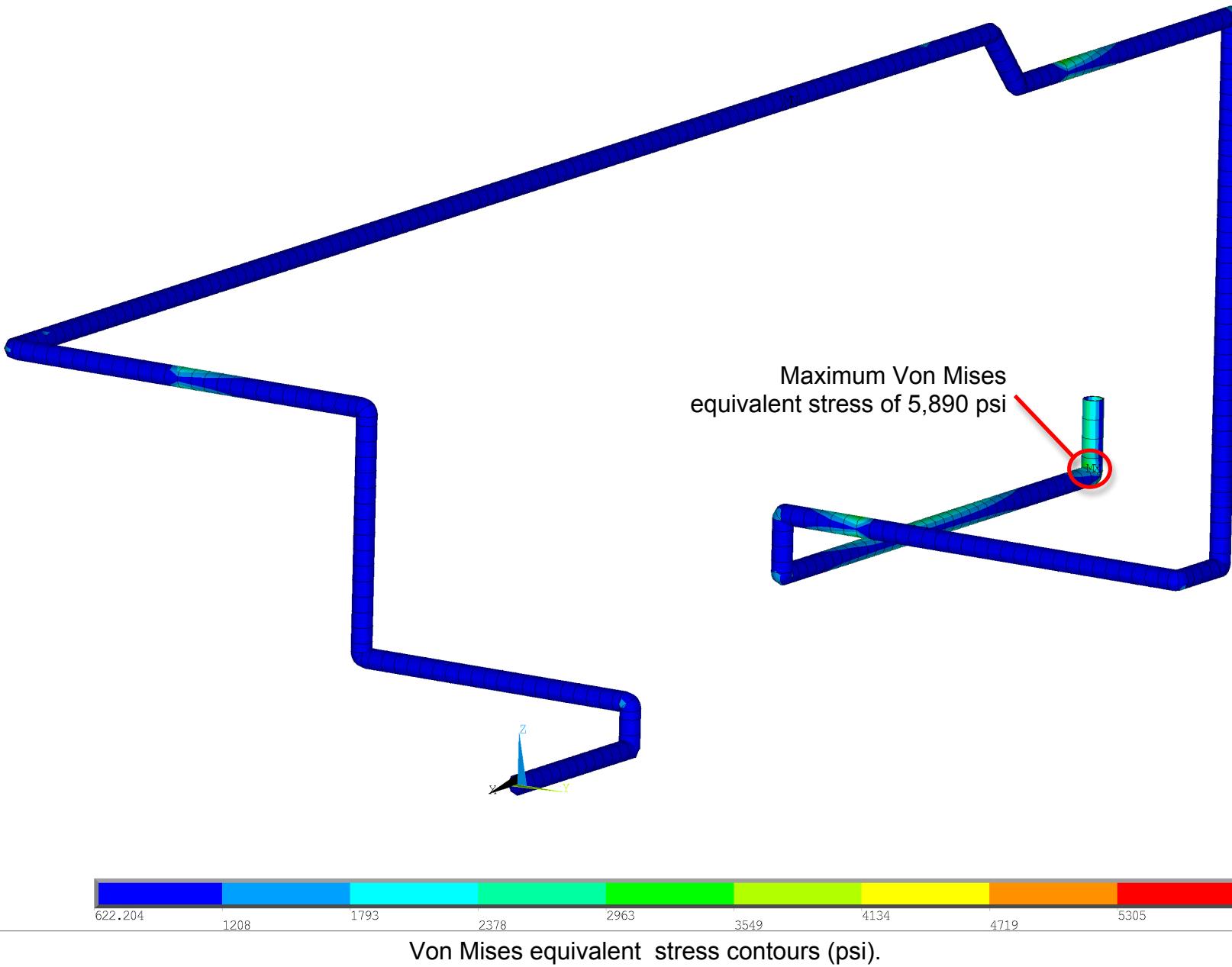
Figure A3.10: GN2 Supply Piping FEA Displacement Contours



1
NODAL SOLUTION
STEP=1
SUB =1
TIME=1
SEQV (AVG)
DMX =1,75
SMN =622,204
SMX =5890

Figure A3.11: GN2 Supply Piping FEA Von Mises Stress Contours

ANSYS
JUL 13 2011
10:30:31
PLOT NO. 1



JUL 13 2011
16:29:32
PLOT NO. 1

1 ELEMENTS
MAT NUM
U
ROT
ACEL

Model info:

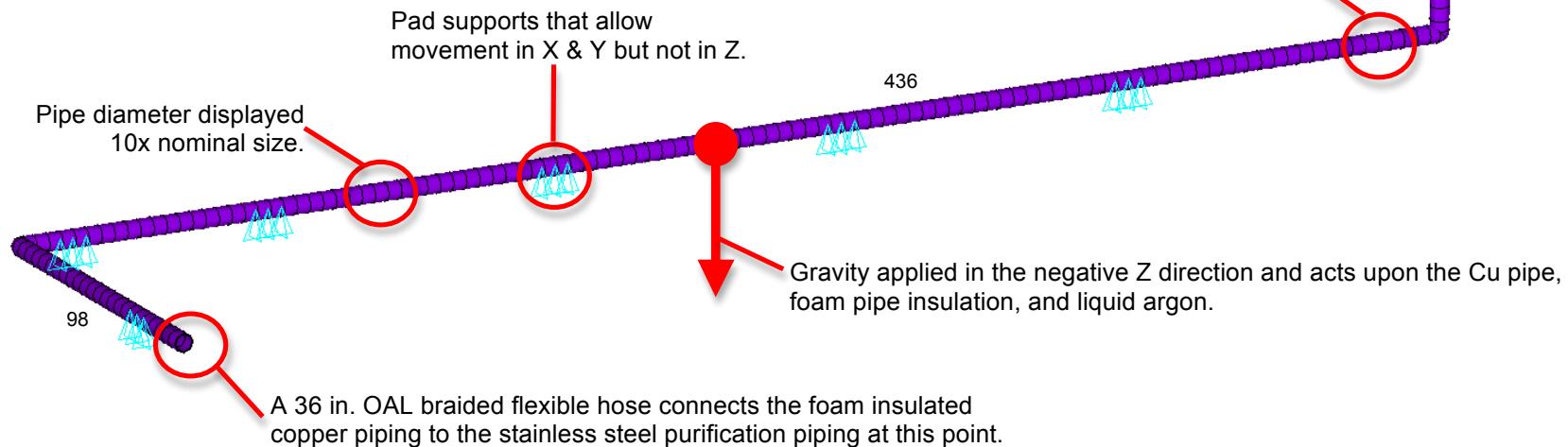
- 1 inch Type K copper pipe, with foam insulation and filled with liquid argon
- 177 ANSYS PIPE16 (straight) and PIPE18 (curved) elements.
- Elbows and tees include B31.3 Stress Intensification Factors.
- Internal pressure of 100 psi applied.
- Model fixed at 70 F and then cooled to -325 F using 3.67 in./100 ft. thermal expansion value for Cu from B31.3 Table C-1 for shrinkage from 70 F to -325 F.
- Young's Modulus of 18.0×10^6 psi used for Cu at -325 F from B31.3 Table C-1. 6

Figure A3.12: Liquid Argon Supply Piping FEA Model

Pipe outside PC4 shrinks towards the PC4 wall in an unrestrained 1D manner

Pipe fixed in XYZ at PC4 wall

Segment length inches

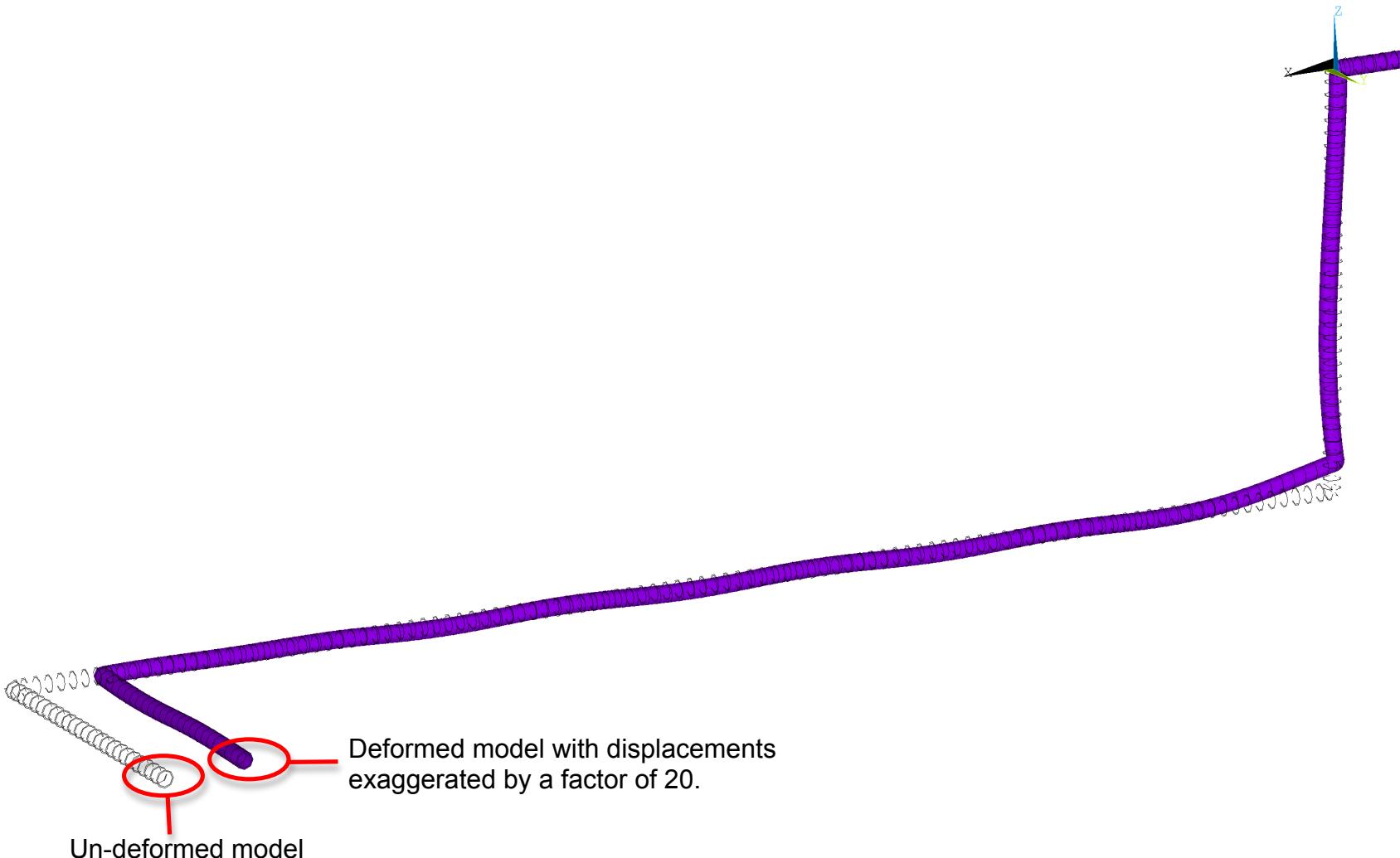


DISPLACEMENT
STEP=1
SUB =1
TIME=1
DMX =1.564

Figure A3.13: Liquid Argon Supply Piping FEA Deformed Shape

ANSYS
JUL 13 2011
16:32:07
PLOT NO. 1

Maximum displacement of 1.5 in. (vector sum).

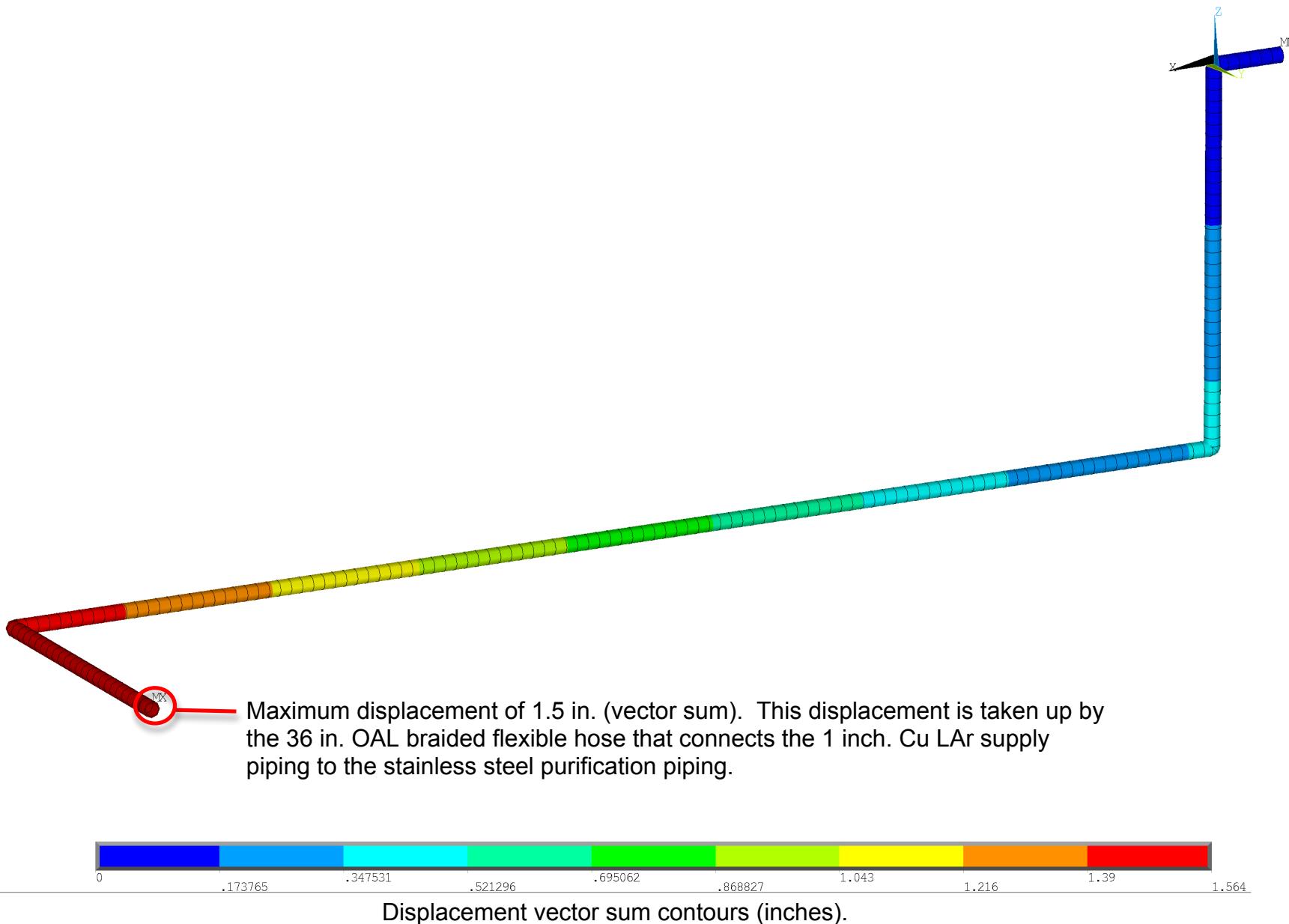


Un-deformed model

1
NODAL SOLUTION
STEP=1
SUB =1
TIME=1
USUM (AVG)
RSYS=0
DMX =1.564
SMX =1.564

ANSYS
JUL 13 2011
16:30:42
PLOT NO. 1

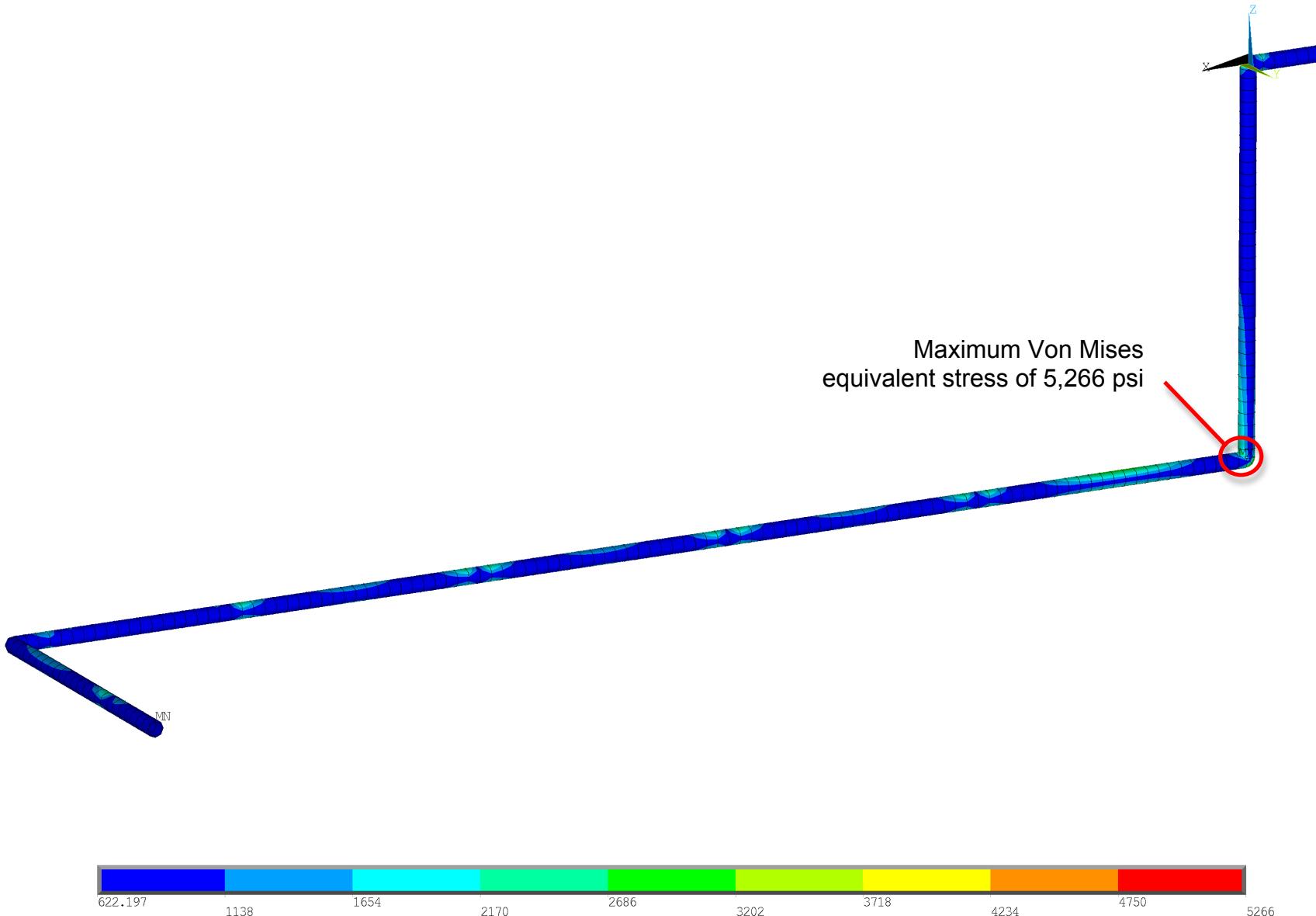
Figure A3.14: Liquid Argon Supply Piping FEA Displacement Contours



1
NODAL SOLUTION
STEP=1
SUB =1
TIME=1
SEQV (AVG)
DMX =1.564
SMN =622,197
SMX =5266

ANSYS
JUL 13 2011
16:30:23
PLOT NO. 1

Figure A3.15: Liquid Argon Supply Piping FEA Von Mises Stress Contours



Appendix 4

Pressure Test

Documentation

The pressure tests required by the amendment will be added to this appendix.



Fermilab

Date: 7/14/11

**EXHIBIT B
Pressure Testing Permit***

Type of Test: Hydrostatic Pneumatic

Test Pressure	110	psig	Maximum Allowable Working Pressure $1.1 \times 100 \text{ psig} = 110 \text{ psig}$	100	psig
---------------	-----	------	--	-----	------

Items to be Tested

LAPD liquid argon supply piping - see attached annotated flow schematic for highlighted test section. Component with the lowest pressure rating is a 150 psig pressure gauge. The piping is rated at 655 psig.

Location of Test PC4 Date and Time _____

Hazards Involved

Stored energy of compressed gas.

Safety Precautions Taken

Test personnel will wear eye protection.

Special Conditions or Requirements

Qualified Person and Test Coordinator
Dept/Date

Terry Tope

PPD/MD/

Division/Section Safety Officer
Dept/Date

Ros Boshell
PD/ES&H

Results

*Held 110 psig for 10 min with no visible drop on the
test gauge. 7/14/11 13329N*

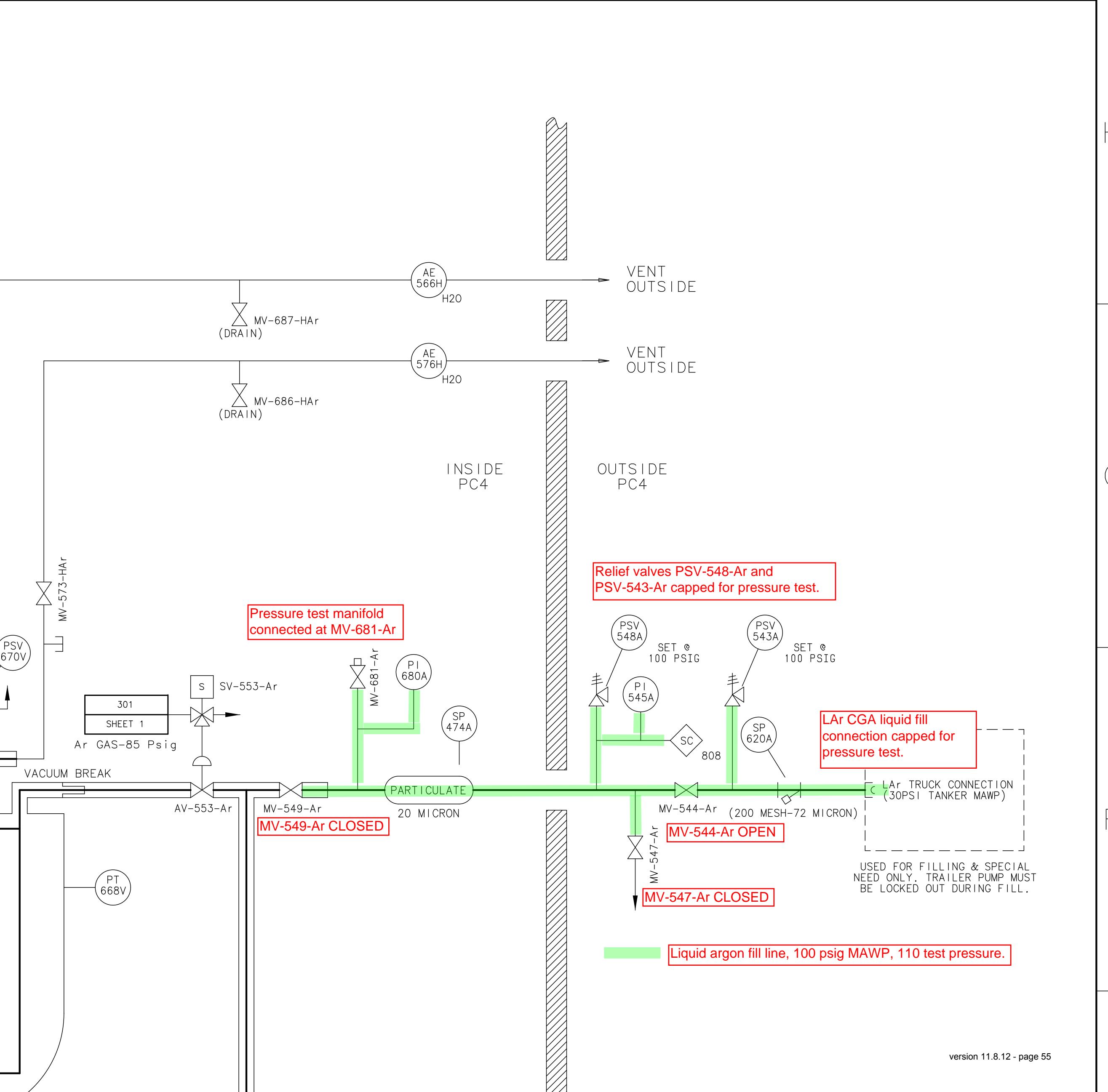
Witness

(Safety Officer or Designee)

Dept/Date

7-15-11

* Must be signed by division/section safety officer prior to conducting test. It is the responsibility of the test coordinator to obtain signatures.





Fermilab

Date: 7/19/11

EXHIBIT B
Pressure Testing Permit*

Type of Test: Hydrostatic Pneumatic

Test Pressure	110	psig	Maximum Allowable Working Pressure	100	psig
1.1 x 100 psig = 110 psig					

Items to be Tested

LAPD liquid nitrogen supply piping - see attached annotated flow schematic for highlighted test section. The piping itself is rated at 655 psig; all other components are rated for at least 100 psig. Phase separator to be tested at a later date.

Location of Test PC4 Date and Time _____

Hazards Involved

Stored energy of compressed gas.

Safety Precautions Taken

Test personnel will wear eye protection.

Special Conditions or Requirements

Qualified Person and Test Coordinator
Dept/Date

Terry Tope
PPD/MD/

Division/Section Safety Officer
Dept/Date

Ros Bushka
PDS/H 7-19-11

Results

Held 110 psig for 10 min. JK

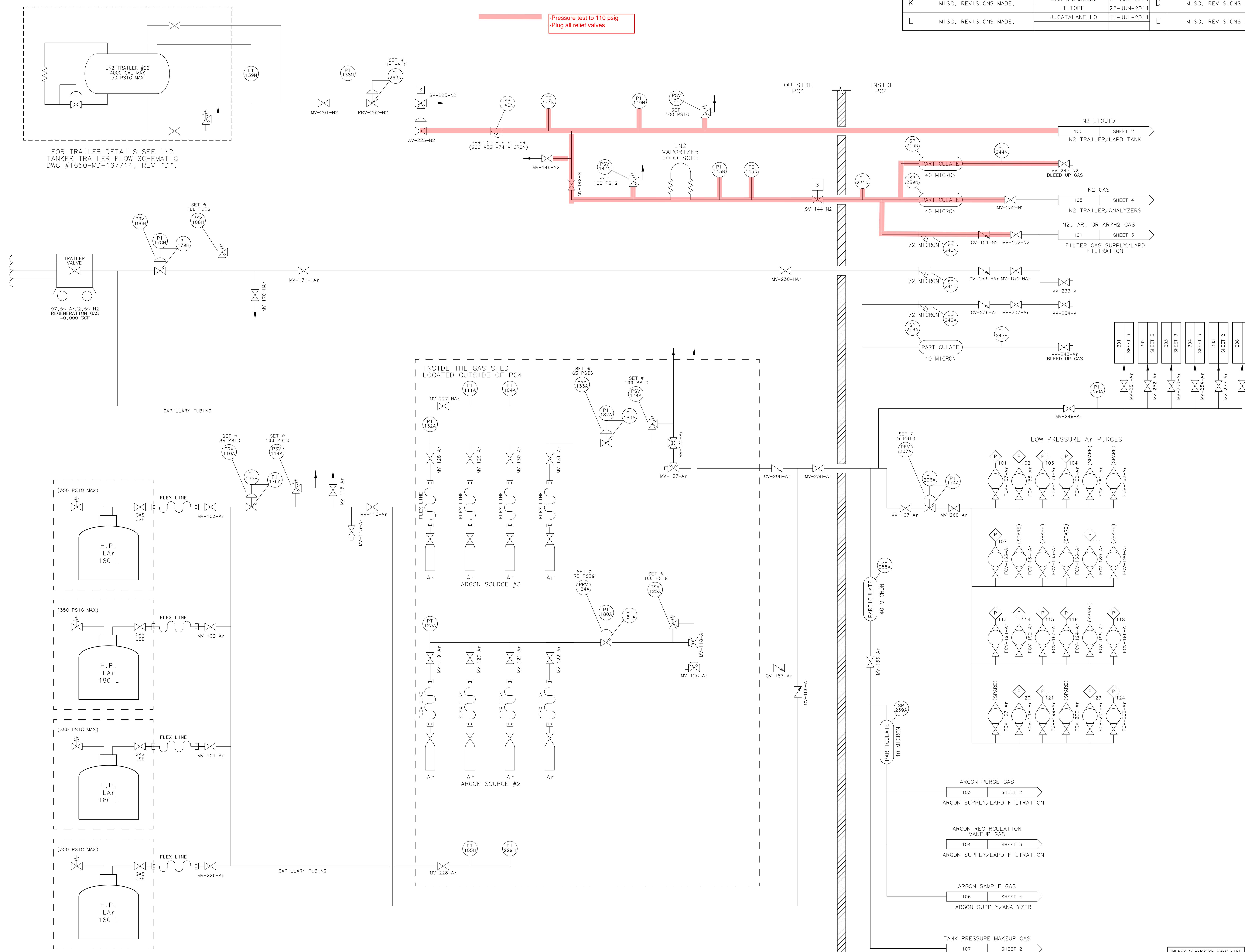
Witness

Ros Bushka 5007N
(Safety Officer or Designee)

Dept/Date

PDS/H 7-19-11

* Must be signed by division / section safety officer prior to conducting test. It is the responsibility of the test coordinator to obtain signatures.



		DRAWN	DATE
		APPROVED	DATE
F	MISC. REVISIONS MADE.	J. CATALANELLO	26-FEB-2010
G	MISC. REVISIONS MADE.	M. ADAMOWSKI	26-FEB-2010
H	MISC. REVISIONS MADE.	J. CATALANELLO	10-JAN-2011
I	MISC. REVISIONS MADE.	T. TOPE	12-JAN-2012
J	MISC. REVISIONS MADE.	J. CATALANELLO	03-FEB-2011
K	MISC. REVISIONS MADE.	J. CATALANELLO	23-FEB-2011
L	MISC. REVISIONS MADE.	J. CATALANELLO	04-MAR-2011
		J. CATALANELLO	22-JUN-2011
		J. CATALANELLO	11-JUL-2011
		J. CATALANELLO	14-DEC-2009
		J. CATALANELLO	17-NOV-2009
		J. CATALANELLO	15-JAN-2010
		T. TOPE	15-JAN-2010

UNLESS OTHERWISE SPECIFIED	ORIGINATOR	R. SCHMITT	26-JUN-2007
DRAWN	J. CATALANELLO	07-DEC-2007	
CHECKED	R. SCHMITT	12-DEC-2007	
APPROVED	R. SCHMITT	12-DEC-2007	
USED ON			
MATERIAL			

1. BREAK ALL SHARP EDGES	MAX.
2. DO NOT SCALE DRAWINGS	DIMENSIONS ARE IN INCHES
3. USE AS IS, UNLESS OTHERWISE SPECIFIED	ASME Y14.3M-1994
4. MAX. ALL MACH. SURFACES	
5. DRAWING UNITS: U.S. INCH	


FERMI NATIONAL ACCELERATOR LABORATORY
UNITED STATES DEPARTMENT OF ENERGY

FLARE UTILITIES
GAS PIPING & INSTRUMENT DIAGRAM
LIQUID ARGON PURITY DEMONSTRAT'N

SCALE DRAWING NUMBER 3942.510-ME-444897 SHEET 1 OF 4 REV L

NONE

CREATED WITH : Ideas2NXSeries GROUP: PPD/MECHANICAL DEPARTMENT



UNLESS OTHERWISE SPECIFIED	ORIGINATOR	R.SCHMITT	26-JUN-2007
DRAWN	J.CATALANELLO	07-DEC-2007	
CHECKED	R.SCHMITT	12-DEC-2007	
APPROVED	R.SCHMITT	12-DEC-2007	
USED ON			
MATERIAL			

5. DRAWING UNITS: U.S. INCH

FLARE UTILITIES
GAS PIPING & INSTRUMENT DIAGRAM
LIQUID ARGON PURITY DEMONSTRAT'N

SCALE DRAWING NUMBER SHEET REV
NONE 3942.510-ME-444897 2 OF 4 L

CREATED WITH: Ideas1NXSeries GROUP: PPD/MECHANICAL DEPARTMENT



Fermilab

Date: 7/20/11

EXHIBIT B
Pressure Testing Permit*

Type of Test: [] Hydrostatic [X] Pneumatic

Test Pressure	66	psig	Maximum Allowable Working Pressure 1.1 x 60 psig = 66 psig	60	psig
---------------	----	------	---	----	------

Items to be Tested

LAPD liquid nitrogen supply piping at phase separator - see attached annotated flow schematic for highlighted test section.

Location of Test

PC4

Date and Time

7/21/11

Hazards Involved

Stored energy of compressed gas.

Safety Precautions Taken

Test personnel will wear eye protection.

Special Conditions or Requirements

Qualified Person and Test Coordinator
Dept/Date

Terry Tope
PPD/MD/

Division/Section Safety Officer
Dept/Date

Ros Bushell
PPES/4 7-21-11

Results

Held 66 psig for 10 minutes w/out drop. *Jesse 13329W*

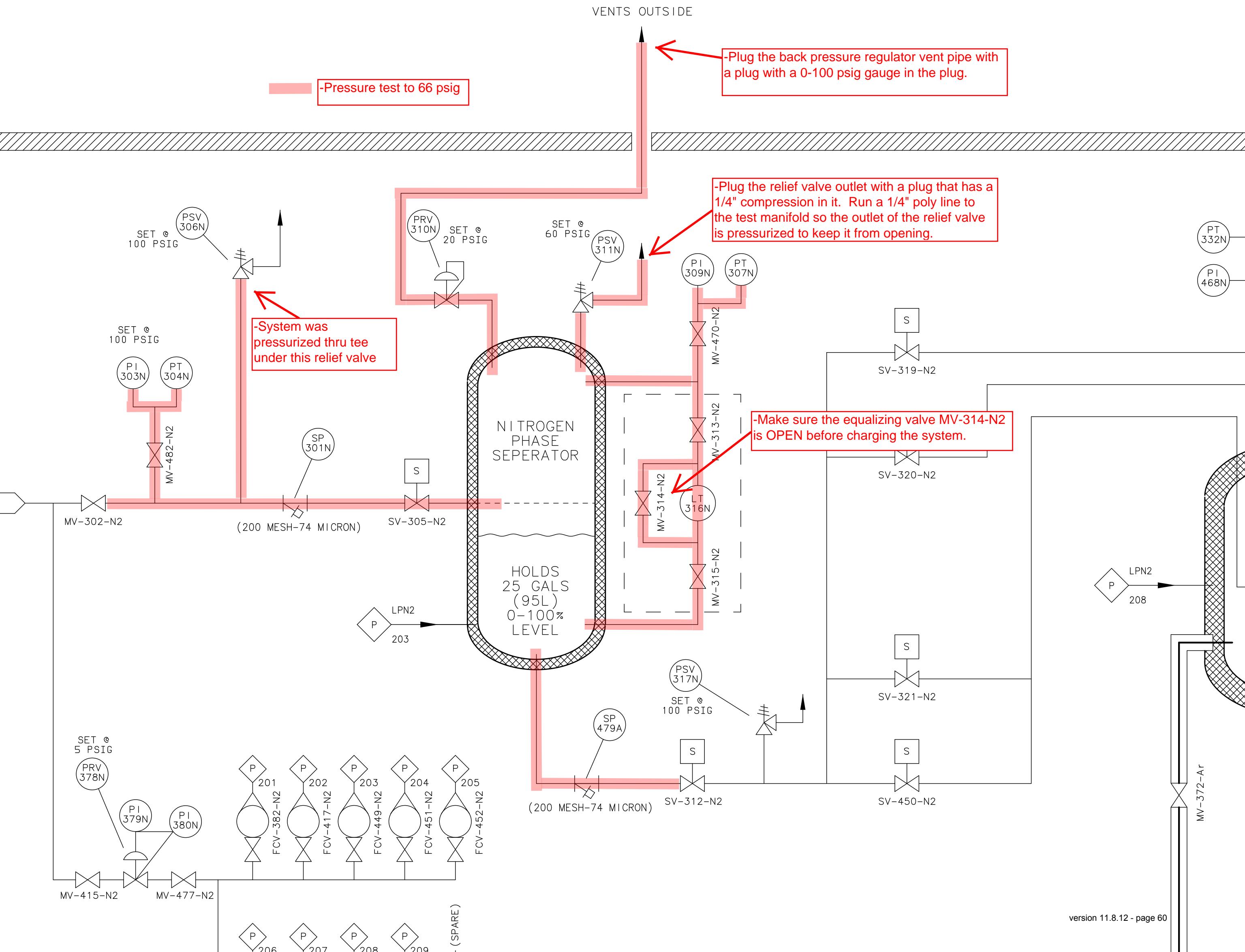
Witness

(Safety Officer or Designee)

Dept/Date

PPES/4 7-21-11

* Must be signed by division/section safety officer prior to conducting test. It is the responsibility of the test coordinator to obtain signatures.





Fermilab

Date: 10/3/12

EXHIBIT B
Pressure Testing Permit*

Type of Test: [] Hydrostatic [X] Pneumatic

Test Pressure	110	psig	Maximum Allowable Working Pressure 1.1 x 100 psig = 110 psig	100	psig
---------------	-----	------	---	-----	------

Items to be Tested

LAPD liquid nitrogen supply piping – see attached annotated flow schematic for highlighted test section. The piping itself is rated at 655 psig – all other components are rated for at least 100 psig. Phase separator to be tested separately at a lower pressure.

FCV-305-N2 and FCV-312-N will slowly leak thru to the phase separator. Phase separator pressure will be monitored.

Location of Test PC4 Date and Time 10/5/12 9:30 AM

Hazards Involved

Stored energy of compressed gas.

Safety Precautions Taken

Test personnel will wear eye protection.

Supply pressure test manifold relieved at 120 psig.

Special Conditions or Requirements

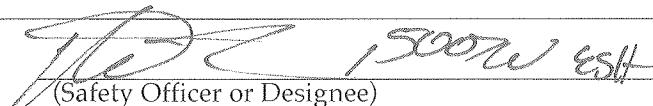
Qualified Person and Test Coordinator Terry Tope
Dept/Date PPD/MD/

Division/Section Safety Officer Rob Bushelk
Dept/Date PPD/ES/H

Results

System held 110 psig. Techs snooped all new /or opened joints @ 100 psig and found no leaks. -Terry Tope 10/3/12 JMB


Witness



10/5/12
(Safety Officer or Designee)

Dept/Date

10-5-12

* Must be signed by division/section safety officer prior to conducting test. It is the responsibility of the test coordinator to obtain signatures.







Date: 10/3/12

EXHIBIT B
Pressure Testing Permit*

Type of Test: [] Hydrostatic [X] Pneumatic

Test Pressure	66	psig	Maximum Allowable Working Pressure 1.1 x 60 psig = 66 psig	60	psig
---------------	----	------	---	----	------

Items to be Tested

LAPD liquid nitrogen supply piping at phase separator – see attached annotated flow schematic for highlighted test section.
Because FCV-305-N2 and FCV-312-N2 leak thru, the piping associated with it will also be at the test pressure.

Location of Test PC4 Date and Time 10/5/12 10:00 AM

Hazards Involved

Stored energy of compressed gas.

Safety Precautions Taken

Test personnel will wear eye protection.

Supply pressure test manifold has a relief valve set just above 66 psig.

Special Conditions or Requirements

Qualified Person and Test Coordinator Terry Tope
Dept/Date PPD/MD/

Division/Section Safety Officer Rob Bushelk
Dept/Date PPD/ES&H


Results

Phase separator held 66 psig. At 60 psig no leaks were detected over a 10 minute period. Terry Tope 1332aw 7/10/12

Witness Terry 150027Wish Dept/Date
(Safety Officer or Designee)

10-5-12

* Must be signed by division/section safety officer prior to conducting test. It is the responsibility of the test coordinator to obtain signatures.



SCALE	DRAWING NUMBER	SHEET	REV
NONE	3942.510-ME-444897	2	4
CREATED WITH : Ideas12NXSeries GROUP: PPD/MECHANICAL DEPARTMENT			
version 11.0.12 - page 60			

Appendix 5

Brazing and Welding

Details

LAPD:
LN2 Supply Brazing Specification

v4.29.10

Terry Tope

(Based on Mathew Cooper's "Booster 95°F LCW System:
Brazing Specification")

1. GENERAL

1.1 Scope

The following specification describes the requirements for brazing (filler metal melting point > 840°F) piping in the LAPD LN2 system. In addition to reinforcement of the key requirements of the governing code listed below, this document specifies supplementary requirements and recommendations relevant to this system to ensure quality brazing.

1.2 Governing Code

All brazing shall be performed in accordance with ANSI/ASME B31.3 Process Piping Code. The LAPD LN2 system shall be considered "Normal Fluid Service" when interpreting Code requirements.

1.3 Inspection Requirements

As set forth in the ANSI/ASME B31.3, in-process examination of brazed joints must be performed.

2. BRAZING MATERIALS

2.1 Filler Metal

The filler metal used is Sil-Fos 15 (high temperature copper-silver-phosphorus alloy brazing filler) for all copper to copper joints. Stainless to copper joints shall use XUPER 1020 XFC silver brazing alloy.

2.2 Flux

There is no flux necessary when using Sil-Fos 15 as the filler metal. The XUPER 1020 XFC silver brazing alloy is coated with the corresponding flux.

3. PREPARATION

3.1 Cleaning

The surfaces to be brazed shall be clean and free from grease, oil, paint, scale and dirt of any kind.

3.2 Fit

The clearance between surfaces to be joined by brazing shall be no larger than necessary to allow complete capillary distribution of the filler metal. Additionally, the material should be completely free of burrs.

4. BRAZING REQUIREMENTS

4.1 Heat Protection

- Sensitive equipment (e.g. cable) must be protected from the heat by the use of heat blankets and shielding where possible.
- Shielding should be used to prevent scorch marks on wall, cabinets, etc.
- Joint shall be brought to brazing temperature in as short a time as possible without localized underheating or overheating

4.2 Gas Purge

To limit oxidation during brazing the piping should be purged with argon.

4.3 Final Finish

All external surfaces in the braze area shall be left in a condition suitable for subsequent inspections (visual, bubble, and hydrostatic pressure tests). The residual soot and/or scale should be removed by wire brush or scouring pad.

5. INSPECTION AND TESTING

5.1 Inspection

As stated in ASME B31.3, not less than 5% of all brazed joints shall be examined by in-process examination, the joints to be examined being selected to ensure that the work of each brazer making the production joints is included. In-process examination comprises examination of the following:

- Joint preparation and cleanliness
- Preheating
- Fit-up, joint clearance, and internal alignment prior to joining
- Variables specified by the joining procedure, including filler material, position, flux, brazing temperature, proper wetting, and capillary action
- Appearance of the finished joint

In-Process Braze Inspection Form

Project: LAPD LN2 Supply

Braze Number: _____

Braze Location: _____

	<u>Acceptable</u>	<u>Not Acceptable</u>
1. Joint preparation and cleanliness	<input type="checkbox"/>	<input type="checkbox"/>
2. Preheating	<input type="checkbox"/>	<input type="checkbox"/>
3. Fit-up, joint clearance, and internal alignment	<input type="checkbox"/>	<input type="checkbox"/>
4. Filler material	<input type="checkbox"/>	<input type="checkbox"/>
5. Position	<input type="checkbox"/>	<input type="checkbox"/>
6. Flux	<input type="checkbox"/>	<input type="checkbox"/>
7. Brazing temperature	<input type="checkbox"/>	<input type="checkbox"/>
8. Proper wetting	<input type="checkbox"/>	<input type="checkbox"/>
9. Capillary action	<input type="checkbox"/>	<input type="checkbox"/>
10. Appearance of the finished joint	<input type="checkbox"/>	<input type="checkbox"/>

Brazer: _____ / _____ Date: _____
(Print) (Sign)

Inspector: _____ / _____ Date: _____
(Print) (Sign)

PPD Mechanical In-Process Weld Inspection Form

(as per In-Process Weld Inspection Guidelines, AD Cryogenics, Nov 3, 2006)

Date _____ Project: _____

Pipe Section: _____ Weld Number: _____

Weld location: _____

Welder: _____ Inspector: _____

Before Welding:

Type of weld: (butt) _____ (other) _____

(1) Pipe #1 Size, Schedule and material: _____

(2) Pipe #2 Size, Schedule and material: _____

(1) Joint Preparation and Cleanliness

Joint Preparation and Cleanliness acceptable? _____

(2) Welding Machine

(a) Remote foot pedal? _____

(b) DC straight machine? _____

(3) Joint Fit-up, and Internal Alignment.

(a) Internal alignment acceptable? _____

(b) Joint Clearance acceptable? _____

(c) End Preparation acceptable? _____

(4) Filler Rod

(a) AWS A5.9 stainless steel filler rod? _____

(b) Filler rod: Class _____ Diameter _____

(5) Purge Gas.

(a) type of purge gas : _____

(b) time length of purge: _____ purge flow rate: _____ SCFH _____

(b) (if done) O2 reading: _____ O2 Monitor manf/model : _____

(6) Inspection After Root Pass

(a) No visible cracks. _____

(b) No suck holes, which are small holes in middle of weld. _____

(c) No porosity or obvious imperfections. _____

(d) Filler material fused along edges of weld . _____

(8) Repeat inspection after every pass: _____

(9) Final Inspection: _____

In-Process Weld Inspection Guidelines
PPD Mechanical Department
(As per AD Cryogenics Department
Nov. 3, 2006)

This procedure is only valid for: GTAW welding of 304SS, 304LSS, 316SS pipe, tube or pipe components such as valves by Fermilab certified welders.

Fermilab welders are certified to weld in any position so there is no need to verify the position when welding. An In-process weld inspection must reflect the WPS for an individual welder.

(1) Joint Preparation and Cleanliness.

Internal and external surfaces to be welded are to be clean and free from rust, oil, grease, dirt, paint, etc. Cleanliness is very important. Even dried residue from a coffee spill is unacceptable and can cause problems. Use scotch bright or Aluminum oxide to clean the joint. Do not use a carbon steel wire brush because it could leave carbon steel particles on the joint.

(2) Welding Machine

- (a) Remote foot pedal required
- (b) DC straight machine required

(3) Joint Fit-up, and Internal Alignment

(a) Internal Alignment:

Butt Weld: The inside surfaces of the two pieces being welded together must be aligned to within 1/32" of each other. If the two pieces are the same outside diameter and wall thickness, then this alignment can be confirmed by using a straight edge on the outside surface.

(b) Joint Clearance

Butt weld: the gap between the two pieces should be less than 1/16".

Socket weld: 1/16" clearance inside the socket.

(c) End Preparation

For butt welds where the wall thickness is over 3/32", prepare pipe ends as per Fig 328.4.2 (attached). If the wall thickness's of the two pipes or tubes differ, prepare their ends as per (attached) Fig 328.4.3.

(4) Filler material

(a) Certification

Filler rod must be AWS designation A5.9 (for stainless).

(b) Record diameter and class (308SS or 304LSS ... etc) of filler rod

(c) Required Filler Rod Class

If connecting	304SS to 304SS	use 308 filler rod
If connecting	304SS to 304LSS	use 308L filler rod
If connecting	304LSS to 304LSS	use 308L filler rod
If connecting	316SS or 304 SS to 316SS	use 316 filler rod

For any other combination consult with the Fermilab weld shop.

(5) Purge Gas

(a) Purity

Purge gas must be 99.995% pure welding grade Argon. Boiloff gas from a liquid argon dewar is acceptable.

(b) Purge Flow

Purge gas must flow through the pipe past weld joint to remove oxygen. As a general rule the preweld purge should give 5-6 volume changes. The attached AWS Fig. 2 chart can be used to determine the required flow rate and length of time of the purge.

(c) Oxygen concentration

Oxygen concentration must be less than 1%. If available, use an oxygen monitor to measure the O₂ concentration of the exhausting purge gas.

(7) Inspection after Root Pass

(a) No visible cracks

(b) No suck holes, which are small holes in middle of weld.

(c) No porosity or obvious imperfections

(d) Filler material fused along edges of weld to parent material. Ideally the weld should be concave.

(8) Repeat inspection #7 above after every pass

(9) Final Pass

Final pass should have a convex shape. Maximum buildup should be less than 1/16" above surface of pipe or tube.



Accelerator Division
Cryogenic Department
630.840.6858 (office)
630.840.4989 (fax)

Memorandum

To: Arkadiy Klebaner, Jay Theilacker, Alex Martinez, Bill Soyars, Brian DeGraff, Jerry Makara, Michael Geynisman

From: Michael White

Subject: Charpy Impact Testing for LN2 Piping

Date: April 13, 2010

Summary of Revision 1

The initial Charpy Impact Testing for LN2 Piping memorandum that was sent on December 29, 2009 contains a known error. The memorandum suggested that welding 316 or 316L with 308L filler metal was acceptable. However, welding 316 or 316L with 308L filler metal is a violation of the AD/Cryo weld procedure, which has now been attached as Appendix 3 to this memo for easy reference. The Charpy impact testing that was performed qualified the AD/Cryo weld procedure for 308L filler rod, but the procedure must be followed to remain within the qualification. All instances where 316 or 316L stainless steel was previously mentioned have been removed, since those materials require the use of 316 filler rod according to the AD/Cryo weld procedure.

It should also be noted that type 308L filler rod also qualifies as type 308, so it is acceptable to weld type 304 to type 304 stainless steel using 308L filler rod even though it is not explicitly specified in the AD/Cryo weld procedure. This memorandum will be updated again once Charpy impact testing data becomes available for welds made with type 316 filler rod using the AD/Cryo weld procedure.

Introduction

The Fermilab Environmental Health & Safety Manual (FESHM) Chapter 5032 stipulates that cryogenic piping must meet the requirements of ASME B31.3. At colder temperatures materials often become brittle and lose their toughness. ASME B31.3 has impact testing requirements that force the designer to ensure that the selected materials do not undergo a brittle transition while being cooled down to the design temperature. Fermilab has had extensive and successful experience with using austenitic stainless steels for cryogenic piping. This paper was written to

demonstrate that all impact testing requirements are satisfied for the vast majority of LN2 piping components at Fermilab through one set of impact tests that were recently performed.

Mandatory Impact Testing

The ASME B31.3 code specifies impact testing instructions in Section 323 and in Table 323.2.2. The two types of stainless steel most commonly used at Fermilab for cryogenic piping are type 304 and type 304L, which are listed in Table A-1 as having a minimum design metal temperature (MDMT) of -425°F (19 K). Table 323.2.2 has two columns of requirements, with column A for materials above their MDMT and column B for materials below their MDMT. The temperature of LN2 at atmospheric pressure is 77 K and well above the MDMT, so the requirements of column B (which are pertinent to LHe piping) will be neglected here.

Column A of Table 323.2.2 is subdivided into two additional columns, with column (a) for the base metal and column (b) for the weld metal requirements. The four types of steel commonly used for cryogenic piping at Fermilab are all austenitic steel, so the appropriate requirements can be found in row 4. Cell A-4(a) specifies that if either (1) carbon content by analysis is > 0.1% or (2) material is not in solution heat treated condition then impact testing is required. Cell A-4(b) specifies that if the MDMT is less than -20°F then the weld metal deposits must be impact tested.

Cell A-4 has two notes, Note (3) and Note (6), which provide exemptions from impact testing. Note (3) only applies above -155°F and therefore is not applicable to LN2 piping. Note (6) exempts material from impact testing if the maximum obtainable Charpy specimen has a width along the notch of less than 2.5 mm (0.098 in). The wall thickness requirements difficult to maintain even if thin-walled tubing or piping is used, since the 2.5 mm wall thickness is often exceeded in the flanges, coupling, and adapters.

One source for stainless steel material composition requirements is ASTM A269-08 “Standard Specification for Seamless and Welded Austenitic Stainless Steel Tubing”, which can be found using links to published standards provided by the Fermilab library. There are various other ASTM standards for stainless steel pipe (such as A312, A358, etc.) but the material composition requirements should be uniform for all ASTM standards. ASTM A269-08 Table 1 specifies that the maximum carbon content is 0.08% for 304 stainless steel and 0.035% for 304L stainless steels.

Section 6 of ASTM A269-08 specifies that the both types of stainless steel must be furnished in solution annealed condition. ASME B31.3 Table A-1 lists all each of the both types of stainless steel as having the same P-No, Group-No, MDMT, and allowable stress regardless of whether it is tube or pipe form. The heat treatment of the tubes and pipes must be similar since the ASME B31.3 listed properties are the same. Therefore, the conditions of cell A-4(a) have been satisfied and impact testing is not required on the base metal when using 304 or 304L stainless steel for LN2 piping.

Cell A-4(b) mandates impact testing on weld metal at LN2 temperatures for 304 or 304L stainless steel if the wall thickness is greater than 2.5 mm. Note (2) applies to all cells in column (b) and states “Impact tests that meet the requirements of Table 323.3.2, which are performed as part of the weld procedure qualification, will satisfy all requirements of para. 323.2.2 and need not be repeated for production welds.” This means that once the AD/Cryo welding procedure is

qualified, no more impact testing is required as long as the weld procedure continues to be followed.

Weld Procedure Qualification

The requirements for impact testing are listed in Table 323.3.1. Since impact tests are only required on the welds, the test is governed by the requirements in column A, cells A-4 to A-7. Cell A-4 states that one impact test is required for each welding procedure, type of filler metal, and flux used. AD/cryo only has one weld procedure, does not use flux for welding, and uses AWS-E308L filler metal so only one test is required. The number of test pieces is dictated by Cell A-5 and Note (3). Note (3) states that the test piece must be large enough to obtain three specimens from the weld metal. Cell A-5(a) states that one test validates a range of thicknesses from T/2 to T+ 0.25". A test on 1" Sch 10 pipe (T=0.109") then would cover the range of 0.055" to 0.359". Almost all fittings and pipe used for LN2 piping at Fermilab fall in this thickness range or below. Cell A-5 states that tests do not need to be repeated as long as the material has the same P-number and Group-number. ASME Boiler Pressure Vessel Code (BPVC) IX QW-422 lists 304 and 304L stainless steels as P-No. 8 and Group-No. 2. Both types of stainless steel typically used by AD/Cryo for LN2 piping will be covered by one set of impact tests.

Cell A-6 gives directions for the orientation and location of the specimens, which will be covered further in the next section. Cell A-7 states that the fabricator (FNAL) is responsible for the ensuring the tests are completed.

Charpy Impact Test Results

FNAL does not have a Charpy impact test facility, so the work was contracted out to Westmoreland Mechanical Testing & Research, Inc (WMT&R) in Youngstown, PA. WMT&R is accredited by the American Association for Laboratory Accreditation (A2LA) to meet ASTM E23 standards for impact testing.

Two 3" long 1" Schedule 10 304 stainless steel pipes were butt welded and sent to WMT&R for impact testing. Impact test specimens were cut and machined by WMT&R. Verbal and written instructions were provided to WMT&R regarding the location and orientation of the specimens. The written instructions included with the welded pipe were the following:

Please follow the instructions from ASME B31.3 Table 323.3.1 on the location and orientation of Charpy Impact test specimens on pipe welds:

Across the weld, with notch in the weld metal; notch axis shall be normal to material surface, with one face of specimen <= 1.5 mm (1/16 in.) from the material surface

Please include the lateral expansion in the test results for all three specimens. ASME B31.3 defines the lateral expansion as:

The increase in width of the broken impact specimen over that of the unbroken specimen measured on the compression side, parallel to the line constituting the bottom of the V-notch

Should you have any questions please contact Mike White at 630-840-6858 or mjwhite@fnal.gov

The AD/Cryo In-Process Weld Inspection form used on the sample sent to WMT&R is included in Appendix 1. The WMT&R test results are included in Appendix 2. ASME B31.3 Table 323.3.5 requires steels with a P-No. of 8 to have at least 0.015" of lateral expansion and has no requirements for dissipated energy. The test results showed that the three specimens had lateral expansion in the range of 0.021"-0.029" at -320°F (77K). All requirements of the Charpy impact test were satisfied.

Conclusion

All Charpy impact testing requirements have been satisfied for using 304 and 304L piping components with 308L filler metal and a wall thickness of less than 0.359". The extensive and successful experience Fermilab has had with the materials listed above has been reinforced with successful Charpy impact testing. No further testing should be required for most LN2 piping assemblies fabricated by AD/Cryo as long as thickness requirements are met.

FERMILAB
Welder Qualification Test Record

COPY

Welder's Name Leonard Harbacek Ident No. 122261 Date 03/19/99

Welding Process GTAW Type Manual

Test in Accordance With WPS # ES-155003 Root Open

Material Specification SA 53-B To Material Specification SA 53-B

P-No 1 To P-No 1 Thickness .280" Diam 6"

Filler Metal Specification SFA A5.18 Classification ER-70S-2 F-No 6

Thickness Deposited .280

Backing Argon Gas Shielding Argon

Position 6-G Progression Upward

Electrical Characteristics: Current DC Polarity Straight

Thickness Qualified .560" Max Diameter Qualified 2-7/8" O.D. and over

GUIDED BEND TEST RESULTS

Specimen No	Type	Figure	Results
1	Face	QW-462.3a	Acceptable
2	Face	QW-462.3a	Acceptable
3	Root	QW-462.3a	Acceptable
4	Root	QW-462.3a	Acceptable

Test Conducted By IFR Engineering Test No. 008-09-01 Date 3/19/99

We certify that the statements in this record are correct and that the test welds were prepared, welded and tested in accordance with the requirements of Section IX of the ASME Code.

By: Leonard Harbacek

Date: 4/22/99

FERMILAB**COPY****Welder Qualification Test Record**Welder's Name Leonard Harbacek Ident No. 122261 Date 03/19/99Welding Process SMAW Type ManualTest in Accordance With WPS # ES-155000 Root OpenMaterial Specification SA 53-B To Material Specification SA 53-BP-No 1 To P-No 1 Thickness .280" Diam 6"Filler Metal Specification SFA A5.1 Classification E6010/E7018 F-No F3/F4Thickness Deposited .280Backing None Gas Shielding N/APosition 6-G Progression UpwardElectrical Characteristics: Current DC Polarity ReverseThickness Qualified .560" Max Diameter Qualified 2-7/8" O.D. and over**GUIDED BEND TEST RESULTS**

Specimen No	Type	Figure	Results
1	Face	QW-462.3a	Acceptable
2	Face	QW-462.3a	Acceptable
3	Root	QW-462.3a	Acceptable
4	Root	QW-462.3a	Acceptable

Test Conducted By IFR Engineering Test No. 008-09-01 Date 3/19/99

We certify that the statements in this record are correct and that the test welds were prepared, welded and tested in accordance with the requirements of Section IX of the ASME Code.

By: Douglas Eller 4/22/99Date: 4/22/99

FERMILAB**COPY****Welder Qualification Test Record**Welder's Name Leonard Harbacek Ident No. 122261 Date 03/19/99Welding Process SMAW Type ManualTest in Accordance With WPS # ES-155000 Root OpenMaterial Specification SA 53-B To Material Specification SA 53-BP-No 1 To P-No 1 Thickness .280" Diam 6"Filler Metal Specification SFA A5.1 Classification E6010/E7018 F-No F3/F4Thickness Deposited .280Backing None Gas Shielding N/APosition 6-G Progression UpwardElectrical Characteristics: Current DC Polarity ReverseThickness Qualified .560" Max Diameter Qualified 2-7/8" O.D. and over**GUIDED BEND TEST RESULTS**

Specimen No	Type	Figure	Results
1	Face	QW-462.3a	Acceptable
2	Face	QW-462.3a	Acceptable
3	Root	QW-462.3a	Acceptable
4	Root	QW-462.3a	Acceptable

Test Conducted By IFR Engineering Test No. 008-09-01 Date 3/19/99

We certify that the statements in this record are correct and that the test welds were prepared, welded and tested in accordance with the requirements of Section IX of the ASME Code.

By: Roger Eller 4/22/99Date: 4/22/99



Fermi National Accelerator Laboratory
 Technical Division-Machine Shop
Welder Performance Qualification Record

Welder's Name	Ryan Mahoney				FNAL #	15470N	ASME #	W-2
Welding Process:	1st	GTAW	Type	Manual	2nd		Type	
Performed in accordance with:		Fermi WPS SS-3,R4						

Joint:	Fillet:	Production Weld			Test Coupon			
Groove:	Double Welded:	Yes	No					
	Single Welded:	Metal Fused	Metal Non Fused	Non-Metal	Open Root	Consumable Insert		
	With Solid Backing	Without Solid Backing						

Base Metal:	Specification:	SA 312, Gr 304	TO	SA 312, Gr 304	ASME P #8	TO	ASME P # 8
Plate		Pipe				Tube	
Actual Thickness:	Nominal Diameter: 4			Actual Diameter: 4/5"	Overall Diameter:		
Qualified Range:	Wt/Schedule: Sch. 80			Qualified Thickness Range: 0-0.674	Wall:		
	Actual Thickness: 0.337			Qualified Diameter Range: 2.875" minimum	Qualified Thickness Range:		
					Qualified Diameter Range:		

Filler:	1 st Process			2 nd Process		
	Specification: SFA 5.9	Class: ER 308/308L		Specification:	Class:	
	Diameter(s): 1/16"Ø, 3/32"Ø			Diameter(s):		
	F #: 6			F #:		
Deposit Thickness: 0.0337	Range Qualification: 0-0.674"		Deposit Thickness:	Range Qualification:		

Welding Position: 6G	If Vertical: Upward Down			
Gas (Type & Composition:	Shielding: Argon 99.9%	Root Side Backing		Argon 99.9%
Electrical Characteristics	Type Current AC DC/EP	DCEN		
	Transfer GMAW	Spray	Globular	Pulse
				Short Circuit

For Information Only		Machine Welding			
Filler Metal Trade Name:		Control:	<input type="checkbox"/> Visual	<input type="checkbox"/> Remote Visual	
SAW Flux Trade Name:		Arc Voltage Control:	<input type="checkbox"/> Auto	<input type="checkbox"/> Other:	
Shielding Gas Trade Name:		Joint Tracking:	<input type="checkbox"/> Yes	<input type="checkbox"/> No	

Visual Inspection					
Appearance:	Satisfactory	Undercut:	Piping Porosity:		

Guided Bend Test					
Type and Figure	Results	Type and Figure	Results	Type and Figure	Results
Test Conducted by:			Lab Test #:		Date:

Radiographic Test					
Results: Satisfactory	Per ASME IX-2007 and AWS D1.1-06				
Radiographer: Alloyweld Inspection Co., Inc.	Examiner: Jennifer Anaya-Level II	Register #5615	Date: 6/18/2010		

Fillet Weld Test Results					
Fracture Test:(Location, Nature, and size of Crack or Tear in Specimen)					
Length of Weld:	Length of Defect:			Percent of Defect	
Macro Test: Fusion					
Appearance: Fillet Size	inch X	inch	<input type="checkbox"/> Convex	<input type="checkbox"/> Concave	
Test Conducted by:			Lab Test #:		

We certify that the statements in this record are correct and that the test welds were prepared, welded, and tested in accordance with the requirements of ASME IX-2007 & AWS D1.1-06 Fermi National Accelerator Laboratory					
By:			Date:		



Fermi National Accelerator Laboratory
Technical Division-Machine Shop
Welder Performance Qualification Record

Welder's Name	Ryan Mahoney				FNAL #	15470N	ASME #	W-2
Welding Process:	1st	GTAW	Type	Manual	2nd		Type	
Performed in accordance with:	Fermi WPS SS-3.R4							

Joint:	Fillet:	Production Weld			Test Coupon		
Groove:	Double Welded:	Yes	No				
	Single Welded:	Metal-Fused	Metal Non-Fused	Non-Metal	Open Root	Consumable Insert	
	With Solid Backing	Without Solid Backing					

Base Metal:	Specification:	SA 312, Gr 304	TO	SA 312, Gr 304	ASME P #8	TO	ASME P # 8
Plate				Pipe	Tube		
Actual Thickness:	Nominal Diameter: 4			Actual Diameter: 4/5"	Overall Diameter:		
Qualified Range:	Wt/Schedule: Sch. 80			Qualified Thickness Range: 0-0.674	Wall:		
	Actual Thickness: 0.337			Qualified Diameter Range: 2.875" minimum	Qualified Thickness Range:		
					Qualified Diameter Range:		

Filler:	1 st Process				2 nd Process			
	Specification: SFA 5.9	Class: ER 308/308L		Specification:		Class:		
	Diameter(s): 1/16" Ø, 3/32" Ø			Diameter(s):				
	F #: 6			F #:				
	Deposit Thickness: 0.0337	Range Qualification: 0-0.674"			Deposit Thickness:	Range Qualification:		

Welding Position:	6G	If Vertical: Upward Down					
Gas (Type & Composition:		Shielding: Argon 99.9%		Root Side Backing		Argon 99.9%	
Electrical Characteristics	Type Current	AC	DCEP	DCEN			
	Transfer GMAW	Spray		Globular	Pulse		Short Circuit

For Information Only		Machine Welding			
Filler Metal Trade Name:		Control:	<input type="checkbox"/> Visual	<input type="checkbox"/> Remote Visual	
SAW Flux Trade Name:		Arc Voltage Control:	<input type="checkbox"/> Auto	<input type="checkbox"/> Other:	
Shielding Gas Trade Name:		Joint Tracking:	<input type="checkbox"/> Yes	<input type="checkbox"/> No	

Visual Inspection		
Appearance:	Satisfactory	Undercut:

Guided Bend Test					
Type and Figure	Results	Type and Figure	Results	Type and Figure	Results
Test Conducted by:	Lab Test #:				Date:

Radiographic Test		
Results: Satisfactory	Per ASME IX-2007 and AWS D1.1-06	
Radiographer: Alloyweld Inspection Co., Inc.	Examiner: Jennifer Anaya-Level II	Register # 5615 Date: 6/18/2010

Fillet Weld Test Results					
Fracture Test:(Location, Nature, and size of Crack or Tear in Specimen)					
Length of Weld:		Length of Defect:		Percent of Defect	
Macro Test: Fusion					
Appearance: Fillet Size	inch X	inch	<input type="checkbox"/> Convex	<input type="checkbox"/> Concave	
Test Conducted by:		Lab Test #:			

We certify that the statements in this record are correct and that the test welds were prepared, welded, and tested in accordance with the requirements of ASME IX-2007 Fermi National Accelerator Laboratory	Date:
	6/18/2010



Fermi National Accelerator Laboratory
 Technical Division-Machine Shop
Welder Performance Qualification Record

Welder's Name	Ryan Mahoney				FNAL #	15470N	ASME #	W-2			
Welding Process:	1st	GTAW	Type	Manual	2nd		Type				
Performed in accordance with:	Fermi WPS SS-3,R4										
Joint:	Fillet:		Production Weld		Test Coupon						
Groove:	Double Welded:	Yes	No								
	Single Welded:	Metal Fused	Metal Non-Fused	Non-Metal	Open Root	Consumable Insert					
	With Solid Backing	Without Solid Backing									
Base Metal:	Specification:	SA 312, Gr 304	TO	SA 312, Gr 304	ASME P #8	TO	ASME P # 8				
Plate	Pipe				Tube						
Actual Thickness:	Nominal Diameter: 4		Actual Diameter: 4/5"		Overall Diameter:						
Qualified Range:	Wt/Schedule: Sch. 80		Qualified Thickness Range: 0-0.674		Wall:						
	Actual Thickness: 0.337		Qualified Diameter Range: 2.875" minimum		Qualified Thickness Range:						
								Qualified Diameter Range:			
Filler:	1 st Process				2 nd Process						
	Specification: SFA 5.9		Class: ER 308/308L		Specification:		Class:				
	Diameter(s): 1/16" Ø, 3/32" Ø				Diameter(s):						
	F #: 6				F #:						
Deposit Thickness: 0.0337		Range Qualification: 0-0.674"		Deposit Thickness:		Range Qualification:					
Welding Position:	6G	If Vertical: Upward Down									
Gas (Type & Composition:	Shielding: Argon 99.9%		Root Side Backing			Argon 99.9%					
Electrical Characteristics	Type	Current	AC	DCEP	DCEN						
	Transfer GMAW		Spray	Globular	Pulse				Short Circuit		
For Information Only				Machine Welding							
Filler Metal Trade Name:			Control:	<input type="checkbox"/> Visual	<input type="checkbox"/> Remote Visual						
SAW Flux Trade Name:			Arc Voltage Control:	<input type="checkbox"/> Auto	<input type="checkbox"/> Other:						
Shielding Gas Trade Name:			Joint Tracking:	<input type="checkbox"/> Yes	<input type="checkbox"/> No						
Visual Inspection											
Appearance:	Satisfactory	Undercut:				Piping Porosity:					
Guided Bend Test											
Type and Figure	Results	Type and Figure	Results	Type and Figure	Results						
Test Conducted by:				Lab Test #:			Date:				
Radiographic Test											
Results: Satisfactory				Per ASME IX-2007 and AWS D1.1-06							
Radiographer: Alloyweld Inspection Co., Inc.				Examiner: Jennifer Anaya-Level II		Register # 5615	Date: 6/18/2010				
Fillet Weld Test Results											
Fracture Test:(Location, Nature, and size of Crack or Tear in Specimen)											
Length of Weld:		Length of Defect:			Percent of Defect						
Macro Test: Fusion											
Appearance: Fillet Size		inch X	inch	<input type="checkbox"/> Convex	<input type="checkbox"/> Concave						
Test Conducted by:		Lab Test #:									
We certify that the statements in this record are correct and that the test welds were prepared, welded, and tested in accordance with the requirements of ASME IX-2007 Fermi National Accelerator Laboratory											
By:							Date:	6/18/2010			



Fermi National Accelerator Laboratory

Technical Division-Machine Shop

Welder Performance Qualification Record

Welder's Name:	<i>Ryan Mahoney</i>			FNAL #:	<i>15470N</i>	ASME #:	<i>W-2</i>
Welding Process:	1st	<i>GTAW</i>	Type:	<i>Manual</i>	2nd		Type:
Performed in accordance with:		<i>Fermi WPS-SS-8-001</i>					

Joint:	Fillet:	Production Weld		Test Coupon		
Groove:	Double-Welded:	<i>Yes</i>	<i>No</i>			
	Single Welded:	<i>Metal Fused</i>	<i>Metal Non-Fused</i>	<i>Non-Metal</i>	<i>Open Root</i>	<i>Consumable Insert</i>
	<i>With Solid Backing</i>	<i>Without Solid Backing</i>				

Base Metal:	Specification:	<i>SA 213, Type 304/304L</i>	TO:	<i>SA 213, Type 304/304L</i>	ASME P #8, Gp I	TO:	<i>ASME P #8, Gp I</i>
Plate	Pipe					Tube	
Actual Thickness:	Nominal Diameter:		Actual Diameter		Overall Diameter: 0.250"		
Qualified Range:	W/U/Schedule:	Qualified Thickness Range		Wall: 0.035"			
	Actual Thickness	Qualified Diameter Range:		Qualified Thickness Range: 0.070" Maximum		Qualified Diameter Range: 0.250" Minimum	

Filler:	1st Process			2nd Process		
	Specification:	<i>5.9</i>	Class:	<i>308/308L</i>	Specification:	Class:
Diameter(s):	<i>.035, .045, 1/16</i>			Diameter(s):		
F #:	<i>6</i>			F #:		
Deposit Thickness:	<i>0.035</i>		Range Qualification:	<i>0.070 Maximum</i>	Deposit Thickness:	Range Qualification:

Welding Position:	<i>6G</i>	If Vertical:	<i>Uphill Down</i>		
Gas (Type & Composition:		Shielding:	<i>Argon 99.9%</i>	Root Side Backing - Argon 99.9%	
Electrical Characteristics	Type Current	AC	DCEP	DCEN	
	Transfer GMAW		Spray	Globular	Pulse
					Short Circuit

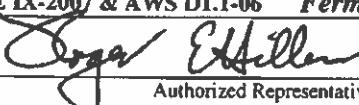
Visual Inspection					
Appearance:	<i>Satisfactory</i>	Undercut:	<i>None</i>	Piping Porosity:	<i>None</i>

Guided Bend Test					
Type and Figure	Results	Type and Figure	Results	Type and Figure	Results
Test Conducted by:	Lab Test #:			Date:	

Radiographic Test					
Results:	<i>Satisfactory</i>		Per ASME IX-2007		
Radiographer:	<i>Alloyweld Inspection Co., Inc.</i>	Examiner:	<i>Jennifer Anaya-Level II</i>	Register #	<i>5615</i>
					Date:

Fillet Weld Test Results						
Fracture Test:						
(Location, Nature, and size of Crack or Tear in Specimen)						
Length of Weld:	Length of Defect:		Percent of Defect			
Macro Test: Fusion						
Appearance: Fillet Size	inch	X	inch	<input type="checkbox"/> Convex	<input type="checkbox"/> Concave	
Test Conducted by:	Lab Test #:					

Test Verified by:	<i>Roger Hiller, 00362N</i>	Verification Report #	<i>5/1/2010-2RH</i>	Signature
--------------------------	-----------------------------	------------------------------	---------------------	------------------

We certify that the statements in this record are correct and that the test welds were prepared, welded, and tested in accordance with the requirements of ASME IX-2007 & AWS D1.1-06 <i>Fermi National Accelerator Laboratory</i>	
By: Roger Hiller 00362N	Date:
	
Authorized Representative	



Fermi National Accelerator Laboratory

Technical Division-Machine Shop

Welder Performance Qualification Record

Welder's Name	Ryan Mahoney				FNAL #	15470N	ASME #	W-2
Welding Process:	1st	GTAW	Type	Manual	2nd		Type	
Performed in accordance with:		Fermi WPS-SS-9-002						

Joint:	Fillet:		Production Weld			Test Coupon	
Groove:	Double Welded:	Yes	No				
	Single Welded	Metal Fused	Metal Non-Fused	Non-Metal	Open Root	Consumable Insert	
	With Solid Backing	Without Solid Backing					

Base Metal:	Specification:	SA 213, Type 304/304L	TO	SA 213, Type 304/304L	ASME P #8, Gp 1	TO	ASME P #8, Gp 1
Plate	Pipe						Tube
Actual Thickness:	Nominal Diameter:			Actual Diameter	Overall Diameter: 0.500"		
Qualified Range:	Wt/Schedule:			Qualified Thickness Range	Wall: 0.095"		
	Actual Thickness			Qualified Diameter Range	Qualified Thickness Range: 0.190" Maximum		
					Qualified Diameter Range: 0.500" Minimum		

Filler:	1 st Process				2 nd Process		
	Specification: 5.9	Class: 308/308L			Specification:	Class:	
	Diameter(s): .045, 1/16, 3/32				Diameter(s):		
	F #: 6				F #:		
Deposit Thickness: 0.095	Range Qualification: 0.190 Maximum			Deposit Thickness:	Range Qualification:		

Welding Position: 6G	If Vertical: Uphill Down						
Gas (Type & Composition:	Shielding: Argon 99.9%	Root Side Backing - Argon 99.9%					
Electrical Characteristics	Type Current AC DCER	DCEN					
	Transfer GMAW	Spray	Globular				Short Circuit

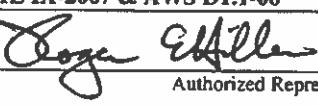
Visual Inspection							
Appearance:	Satisfactory	Undercut:	None		Piping Porosity:	None	

Guided Bend Test							
Type and Figure	Results	Type and Figure	Results	Type and Figure	Results		
Test Conducted by:	Lab Test #:				Date:		

Radiographic Test							
Results: Satisfactory	Per ASME IX-2007 and AWS D1.1-06						
Radiographer: Alloyweld Inspection Co., Inc.	Examiner: Jennifer Anaya-Level II	Register # 5615	Date: 6/18/2010				

Fillet Weld Test Results							
Fracture Test: (Location, Nature, and size of Crack or Tear in Specimen)							
Length of Weld:	Length of Defect:			Percent of Defect			
Macro Test: Fusion							
Appearance: Fillet Size	inch X	inch		<input type="checkbox"/> Convex	<input type="checkbox"/> Concave		
Test Conducted by:	Lab Test #:						

Test Verified by: Roger Hiller 00362N	Verification Report #5272010-2	Signature
---------------------------------------	--------------------------------	-----------

We certify that the statements in this record are correct and that the test welds were prepared, welded, and tested in accordance with the requirements of ASME IX-2007 & AWS D1.1-06 Fermi National Accelerator Laboratory			
By: Roger Hiller 00362N  Authorized Representative		Date:	6/18/2010